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A General Procedure for Obtaining Velocity
Vector from a System of High Response Impact
Pressure Probes

D. Adler and R. P. Shreeve

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<p>A technique to measure a high frequency, repetitively pulsating flow field is presented. Two impact tube probes and a Kiel probe, all with pressure transducers mounted in their tips are used. Five readings are required to identify a velocity vector at a point.</p> <p>In this report the technique, the numerical procedure and the computer program used are described.</p>

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A General Procedure for Obtaining Velocity

Vector From a System of High

Response Impact Pressure Probes

by

D. Adler and R. P. Shreeve

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Notation

- C_p - Pressure coefficient defined in eq. (3)
- α - Yaw angle relative to laboratory space
- ϕ - Pitch angle relative to laboratory space
- P_t - Total pressure
- P_s - Static Pressure
- α_{rp} - Yaw angle relative to probe axis
- ϕ_{rp} - Pitch angle relative to probe axis
- P_p - Pressure indicated by the probe
- α_p - Yaw setting of the probe
- ϕ_p - Pitch setting of the probe

Subscripts

- I }
II } relating to probe positions shown
III } in figure 3
IV }
- A relating to A type probe
- B relating to B type probe
- Lo lowest value in an array
- rp relative to the probe axis
- Up highest value in an array

Notation of PENPTS

- DD - denominator in the subsequent line of the program
- HT - penetration height (C_p of a calibration surface)
- IR - a flag with a value of either 1 or 2 to identify first or second penetration point. This flag also controls return of values to calling program or subroutine
- IB - a flag indicating the location of the last rectangle in the band checked for a penetration point. It prevents repetition of the scanning in the 103 Do loop
- NX - number of X values in the calibration surface grid (\approx values of the calibration surface)
- NY - number of Y values in the calibration surface grid (\approx values of the calibration surface)
- X(I) - X values in the grid
- XM - value of X at point B (fig. 5)
- XR(I) - two values of X returned by the subroutine as results
- XS - currently calculated value of X which is the present result and is later stored in XR(I)
- Y(J) - Y values in the calibration grid
- YC - intermediate value used in the subsequent line of the program
- YG - the Y position of the penetrating line*
- Z(I,J)- Values of the $Z = C_p$ calibration surface above grid points
- ZX - value of Z either at point A or point C (see figs. 5, 6 and 7)
- ZM - value of Z at point B

* It should be pointed out here that the penetrating line is parallel to the X axis at a height $HT = C_p$ above the X,Y plane and at a distance YG from the X axis on the X,Y plane

Notation of INTSCS

AA	- constant defined in eq. 8
AB	- constant defined in eq. 9
ARIN	- ordinate at which scanning starts
ARLO	- lowest ordinate of calibration surface (as a condition it must be identical for all calibration surfaces used)
ARM1	- ordinate measured relative to probe 1 (the probe belonging to the first curve $C_p = \text{const.}$)
ARM2	- ordinate measured relative to probe 2 (the probe belonging to the second curve $C_p = \text{const.}$)
ARP1	- setting ordinate of probe 1
ARP2	- setting ordinate of probe 2
ARRES (1)	- abscissa value returned to INTSCS from PENPTS
ARUP	- highest ordinate of calibration surface (as a condition it must be identical for all calibration surfaces used)
AR2R	- ordinate relative to laboratory space
AR2RJ	- ordinate relative to laboratory space of previous scan
BA	- constant defined in eq. 8
BB	- constant defined in eq. 9
DAR	- ordinate step for scanning
HT1	- penetration height of calibration surface of probe 1 (C_p of probe 1)
HT2	- penetration height of calibration surface of probe 2 (C_p of probe 2)
IEPS	- a flag which is equal to 2 when the calculation is carried out as shown in fig. 11, otherwise it is equal to 1. (This information is required in the main program and is returned to it)

ISL	- a flag which is equal to 10 if one of the left hand side results returned from PENPTS is 1000.0 (i.e., is not a penetration point). Otherwise it is equal to 1
ISR	- a flag which is equal to 10 if one of the right hand side results returned from PENPTS is 1000.0 (i.e., is not a penetration point). Otherwise it is equal to 1
K	- a flag indicating whether the first or the second intersection is evaluated
N1	- number of abscissas in calibration surface grid (fig. 4)
N2	- number of Ordinates in calibration surface grid (fig. 4)
RES1(K)	- evaluated and returned abscissa of intersection
RES2(K)	- evaluated and returned ordinate of intersection
R1	- radius in fig. 11 for probe 1
R2	- radius in fig. 11 for probe 2
RAIL	- abscissa of point AIL in fig. 9 or 10
RAIR	- abscissa of point AIR in fig. 9 or 10
RAJL	- abscissa of point AJL in fig. 9 or 10
RAJR	- abscissa of point AJR in fig. 9 or 10
RBIL	- abscissa of point BIL in fig. 9 or 10
RBIR	- abscissa of point BIR in fig. 9 or 10
RBJL	- abscissa of point BJL in fig. 9 or 10
RBJR	- abscissa of point BJR in fig. 9 or 10
X1(I)	- abscissas of calibration surface of probe 1 or its transformation as determined by calling statement in main program
X2(I)	- abscissas of calibration surface of probe 2 or its transformation as determined by calling statement in main program

$X3(I)$ - abscissas of calibration surface of probe 1 or its transformation as determined by calling statement in main program
 $X4(I)$ - abscissas of calibration surface of probe 2 or its transformation as determined by calling statement in main program
 $Y1(I)$ - ordinates matching $X1(I)$
 $Y2(I)$ - ordinates matching $X2(I)$
 $Y3(I)$ - ordinates matching $X3(I)$
 $Y4(I)$ - ordinates matching $X4(I)$
 $Z1(I,J)$ - values of Cp_{rp} for $X1(I)$ and $Y1(I)$
 $Z2(I,J)$ - values of Cp_{rp} for $X2(I)$ and $Y2(I)$
 $Z3(I,J)$ - values of Cp_{rp} for $X3(I)$ and $Y3(I)$
 $Z4(I,J)$ - values of Cp_{rp} for $X4(I)$ and $Y4(I)$

Notation of Main Program VDR

A	- variables in library routine IXCLOK used to evaluate computation times
ALF	- values of α returned to VDR from INTSCS
ALFA	- α input when experiment simulation is carried out
ALFC	- α_{rpIII}
ALFCN	- new value of α_{rpIII} for next iteration
ALFD	- α_{rpIV}
ALFDN	- new value of α_{rpIV} for next iteration
ALF1	- α_I
ALF2	- α_{II}
ALF3	- α_I
ALF4	- α_{III}
AM	- mach number
CPA	- $C_{p_{rpI}}$
CPB	- $C_{p_{rpII}}$
CPC	- $C_{p_{rpIII}}$
CPD	- $C_{p_{rpIV}}$
EPSPS	- relative difference between present static pressure and its value in the previous iteration
EPSPSG	- convergence criterion (on the static pressure)
FALF	- final α value (at convergence)
FPHI	- final ϕ value (at convergence)
IA50	- a flag in IXCLOK
IA60	- a flag in IXCLOK
ICOPS	- number of PS corrections carried out to ensure the C_p 's are in calibration range
IEPS	- a flag governing the convergence criterion returned from INTSCS

IEPS1 - a flag governing the convergence criterion for probes I and II
 IEPS2 - a flag governing the convergence criterion for probes I and III
 IIT - number of iterations on p_s
 ISCAN - number of static pressure scans from initial static pressure guess upwards
 IXCLOK - system subroutine for computation time evaluation
 NOCOPS - a flag which when equal to 1 causes static pressure corrections to be carried out such that C_p 's are always inside calibration range, and when equal to 2 cause these corrections to be skipped
 NOSIM - a flag which when equal to 1 causes the program to simulate velocity measurement experiments and when equal to 2 causes the program to reduce measured data
 NX - number of calibration surface matrix abscissa's, α values (must be identical for all calibration surface matrices used)
 NY - number of calibration surface matrix ordinates, ϕ values (must be identical for all calibration surface matrices used)
 PDYN - dynamic pressure
 PHI - value of ϕ returned to VDR from INTSCS
 PHIB - ϕ_{rpII}
 PHII - ϕ input when experiment simulation is carried out
 PHI1 - ϕ_{rpI}
 PHI2 - ϕ_{rpII}
 PHI3 - ϕ_{rpI}
 PHI4 - ϕ_{rpIII}
 PPA - signal of probe in position I
 PPB - signal of probe in position II

PPC - signal of probe in position III
 PPC - signal of probe in position IV
 PS - static pressure
 PSIN - initial guess of static pressure
 PSN - new value of static pressure for next iteration
 PSC - corrected static pressure
 PST - memorized corrected static pressure
 PT - total pressure measured
 RELXPS - relaxation factor for convergence on the static pressure
 VIRTIM - virtual computation time
 XA - abscissas of calibration surface matrix of probe A
 XAX - transformed abscissas of calibration surface matrix of probe A
 XB - abscissas of calibration surface matrix of probe B
 XBX - transformed abscissas of calibration surface matrix of probe B
 XPC - yaw setting of position III
 XPD - yaw setting of position IV
 XRIN - α value at which scanning starts
 XRLU - lowest α value of calibration surface (as a condition it must be identical for probes A and B)
 XRUP - highest α value of calibration surface (as a condition it must be identical for probes A and B)
 YA - ordinates of calibration surface matrix of probe A
 YAX - transformed ordinates of calibration surface matrix of probe A
 YB - ordinates of calibration surface matrix of probe B
 YBX - transformed ordinates of calibration surface matrix of probe B

YPA	- pitch setting of probe A
YPB	- pitch setting of probe B
YRIN	- ϕ value at which scanning starts
YRLO	- lowest ϕ value of calibration surface (as a condition it must be identical for probes A and B)
YRUP	- highest ϕ value of calibration surface (as a condition it must be identical for probes A and B)
ZA	- Cp_{rpA} values of probe A
ZAX	- transformed Cp_{rpA} values of probe A
ZAMAX	- maximum of ZA array
ZAMIN	- minimum of ZA array
ZB	- Cp_{rpB} values of probe B
ZBX	- transformed Cp_{rpB} values of probe B
ZBMAX	- maximum of ZB array
ZBMIN	- minimum of ZB array

Introduction

Experimental knowledge of the flow field generated by rotating turbo impellers is of prime importance in the research and development of turbomachinery. It is essential for the refinement of design methods, for the development of new flow models which include secondary flow and tip clearance effects, and particularly for the verification of new computer codes developed to calculate the flow through rotating blade rows.

In recent years laser velocimeter techniques have been applied successfully to measure the flow both inside and downstream of rotors. (Ref. 1 for example). It has become clear however, that the laser techniques are only reliable in the hands of experienced investigators. A window which remains clean is essential, and seeding is usually required. Laser techniques do not measure the pressure field and usually can only measure two components of the velocity unless the axis of the laser is tilted. Difficulty is also encountered when measuring close to walls. Hence there are reasons to consider alternative techniques, particularly if they are simpler to apply routinely in stationary turbomachinery passages. Furthermore, the achievement of redundancy in measuring the flow field behind the impeller is itself a worthwhile goal. The present

work deals with the application of a particular system of small high response pressures probes at the exit of an impeller.

Measurements behind an impeller, in the stationary bladeless gap, are simpler to make than measurements within the rotating passages. Transducer probes can be installed through the stationary machine casing and the data transmitted without resort to slip rings or rotary transformers. The sensor is not subjected to the centrifugal field or to the vibration of the rotor. However, the flow to be measured is then fluctuating at blade-passing frequency and any system of sensors must be calibrated for a wide range of possible Mach number, pitch angle, yaw angle and pressure variation - and yet must be capable of the necessary frequency response.

In Ref. 2, a method was described for using two semiconductor pressure probes together with the technique of synchronized sampling, to obtain the distribution of the velocity vector downstream of a rotor. The geometries of the two probes, designated Type A and Type B, and their installation in the compressor annulus are shown in Fig 1. It was argued that, in principle, by rotating the probes in yaw about their tips and controlling the sampling of the data from each probe to be at the same position in the rotor frame, the system of two separate probes could be used to acquire data at a point in the periodic flow

TYPE A PROBE

TYPE B PROBE

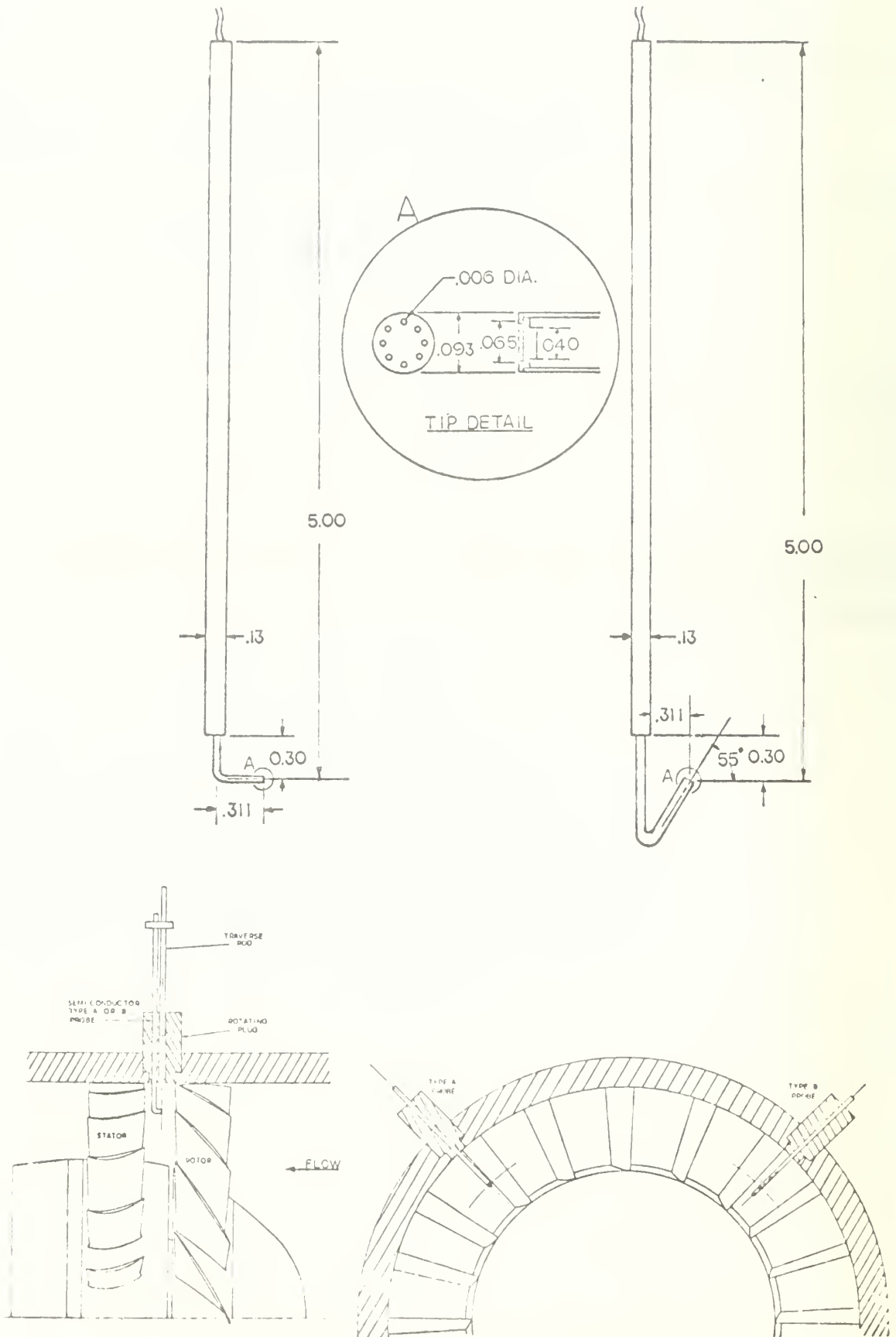


FIGURE 1. TYPE A AND TYPE B PROBES AND COMPRESSOR INSTALLATION.

from the rotor, corresponding to data normally obtained from the multiple sensors of four- or five hole pneumatic probes when measuring velocity in steady flows. The technique promised the use of probes having the simplest geometry and thus avoided the large size, expense and unreliability of multiple sensor probes which incorporate multiple semi-conductor transducers (Ref. 3). Because of the simple sensor tip geometry (that of a cylinder at incidence to the flow) the unsteady response was likely to be as good as could be expected of any single physical sensor.

The two-probe technique is strictly applicable only to periodic flows. However, data obtained on successive rotations of the rotor can be averaged to eliminate fluctuations which are not periodic. This was shown to be effective in tests reported in Ref. 2 in which a single Type A probe was used to establish the peripheral blade-to-blade distribution of flow yaw angle.

In order to obtain velocity from the pressure measurements which can be obtained from the two probes, the steady response characteristics must first be established in calibration tests carried out in a known, controlled, uniform flow. Second, a method of applying the calibration to measurements made in an unknown flow must be devised. In the present method two different approaches have been followed. In Ref. 4, a technique is given for representing

and applying the probe calibration analytically. When first applied the method gave surprisingly good accuracy (1 - 2%) since the method required that the probes had characteristics which could be well represented analytically. This in turn required that the probe tips be geometrically precise, a feature which was not present in the first generation of probes.

A second, more general approach is reported here, wherein the calibration of each probe is represented by a two-dimensional array of pressure coefficients. The application of the calibration given in this form, in an unknown flow required the development of special numerical procedures. The purpose of the present report is to document the analysis and the Fortran program developed to apply the method.

In its present form, the method does not require that the calibration "Surfaces" be symmetrical about any axis or be expressed in analytical form, but does require that the pressure coefficient be independent of Mach number. The latter restriction could undoubtedly be removed by introducing additional iterative steps. Further, in the present method only five measurements have to be taken to determine uniquely a velocity vector at a point. Throughout the report, the Fortran program notation has been used to describe the physics and equations involved in the solution.

Mathematical model

Assume the A and B type probes of ref. [1] (see also fig. 1) to be immersed in a three-dimensional steady flow field.* The pressure response of each of these probes in given gas is functionally described by four variables as:

$$P_p = P_p (\alpha, \phi, P_T, P_S) \quad (1)$$

If a pressure coefficient is defined as

$$Cp_{rp} = \frac{P_p - P_s}{P_T - P_s} \quad (2)$$

The calibration surface of each probe is given in the general case in form of a matrix of values of Cp , where

$$Cp_{rp} = Cp_{rp}(\alpha_{rp}, \phi_{rp}) \quad (3)$$

The pressure coefficient defined in this way has only a second order dependence on Mach and Reynolds numbers in the range of

* For our purpose, using the synchronized sampling, the flow field behind the impeller is steady, although the probes require a high speed response because of fluctuations.

$0 < Ma < 0.7$ in turbulent flows (Ref. 2), so that, to first order their influence is neglected in writing eq. (3).

If the type A probe is rotated about its axis into three different positions ($i = I, III, IV$) readings are taken, and the type B probe is fixed in position II and a single reading is taken, the following four equations can be written.

$$\begin{aligned} C_{p_{Ai}} &= \frac{P_{p_{Ai}} - P_S}{P_T - P_S} = C_{p_{Ai}}(\alpha, \phi) \\ C_{p_{BII}} &= \frac{P_{p_{BII}} - P_S}{P_T - P_S} = C_{p_{BII}}(\alpha, \phi) \end{aligned} \quad (4)$$

it should be pointed out here, to avoid misunderstanding that α and ϕ are defined in a coordinate system relative to the machine axis and not relative to the probe axis. In the set of four equations (4) there are four unknown quantities, namely: α , ϕ , P_T and P_S . These are the quantities to be evaluated using the measured data. Together with the stagnation temperature they define the flow field uniquely. The four equations, resulting from the four measurements, should be sufficient to determine the four unknown quantities.

But the problem is complicated by three facts:

- 1) The calibration surfaces are not generally known in analytical form.
- 2) The calibration surfaces are double valued in α and ϕ i.e., for a given C_p and α there exist two ϕ values, or for a given C_p and ϕ there are two α values which satisfy eq. 3.

- 3) As a result of the measurement the value of P_p rather than of C_p is determined.

Since the calibration surfaces are not given in a simple analytical form the solution has to be numerical. An iterative procedure is required because P_p and not C_p values are measured. First P_s and P_T have to be guessed to yield C_p values, knowing the four measured values of P_p , and using eq. 4. The guess is then iteratively corrected to converge on the solution. However, convergence of the iterative procedure is complicated because of the double valued nature of the calibration surfaces.

This method of iteration shown in Fig. 2 was attempted initially for the evaluation of a measured point. In practice the initially suggested procedure converged in some cases and diverged in others, depending on the values, and signs of α and ϕ . This was not surprising as convergence on two variables is not likely to be a simple matter. However, in order that the measurement technique be useful, convergence on the correct solution for a general set of measurements, is absolutely necessary. In practice, this can certainly be achieved if one of the two iteration variables is obtained by measurement. Since the static pressure is a difficult quantity to measure even in a steady flow field, only the stagnation pressure measurement need be considered. It is possible that the time-varying stagnation pressure could be measured with a suitably designed Kiel probe. Data would then be taken by synchronized sampling from the fixed Kiel probe, from the type A probe rotated into two positions, and from the

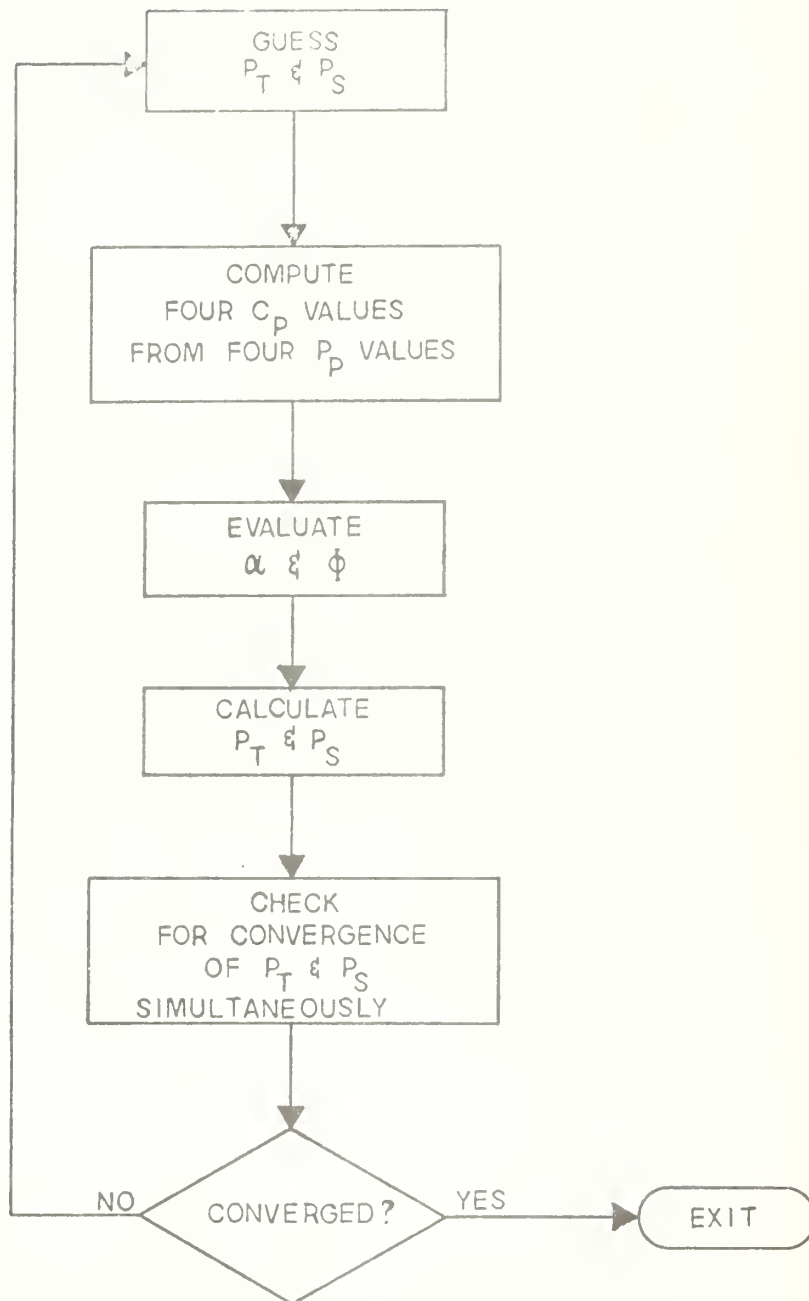


Fig. 2: Unstable iterative solution using measurement of A type and B type probes only.

fixed type B probe. The method of solution is then as shown in Fig. 3. The method shown in Fig. 3 proved to converge under all conditions. It is described in detail in the following pages.

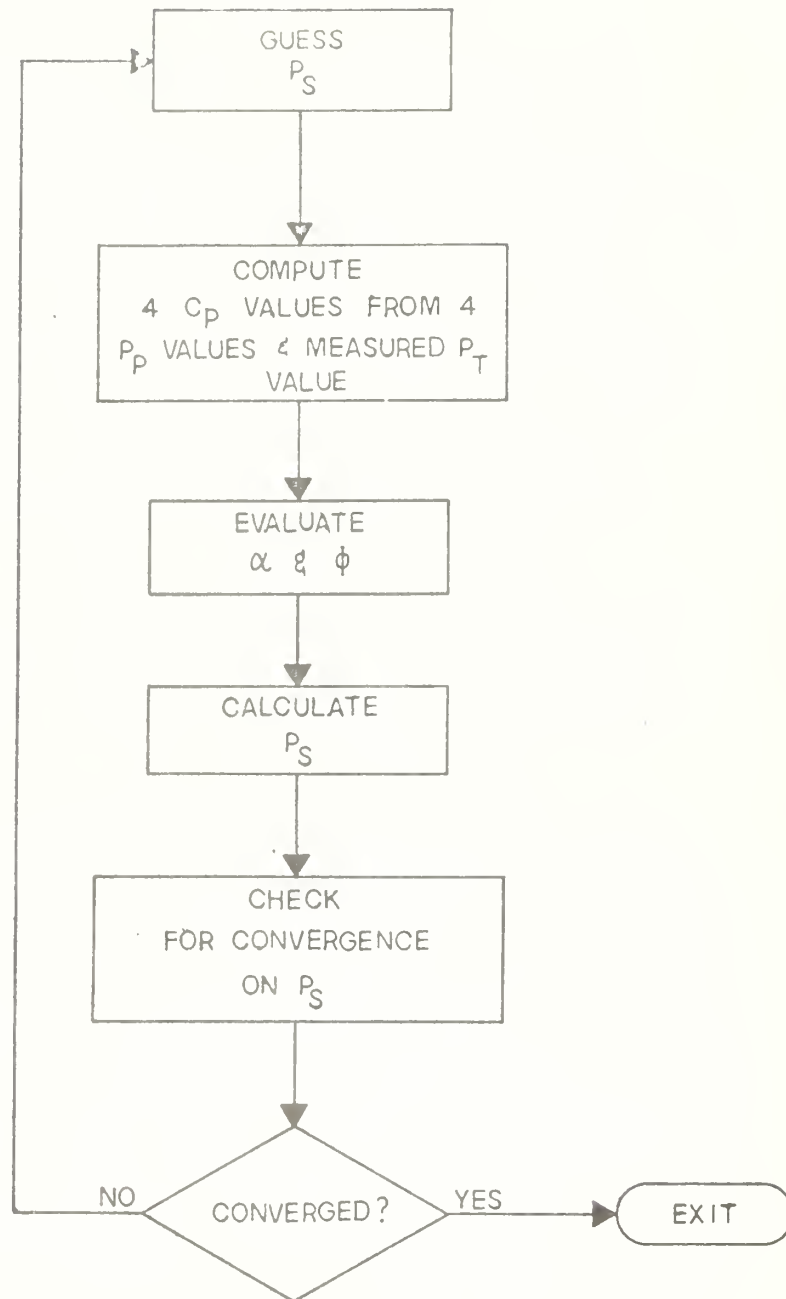


Fig. 3: Stable iterative solution using measurements of A type and B type probes as well as measurements of a Kiel probe.

Evaluation of α and ϕ (method)

The best way to understand the evaluation of yaw and pitch is to look at it from a topographical point of view. Each of the type A and type B probes has a unique calibration surface $Cp_{rp} = Cp_{rp}(\alpha_{rp}, \phi_{rp})$, where α_{rp} and ϕ_{rp} are measured relative to the axis of symmetry through the sensor at the probe tip. The calibration surface in this representation is invariant to yaw and pitch of the probe axis relative to the laboratory space. The same calibration surface if represented in the form $Cp = Cp(\alpha, \phi)$ can be written as

$$Cp = Cp[(\alpha_p + \alpha_{rp}), (\phi_p + \phi_{rp})] \quad (5)$$

where α_p and ϕ_p are the probe tip axis angular settings relative to the laboratory space. It is clear from eq. (5) that Cp can be derived from Cp_{rp} by a constant translation: α_p , ϕ_p on the α, ϕ plane. As each Cp_{rp} can be viewed as a hill with its peak at $\alpha_{rp} = 0$ and $\phi_{rp} = 0$. The Cp surfaces are the same hills with their peaks translated to $\alpha = \alpha_p$ and $\phi = \phi_p$.

In the present method probe A is used in three different angular settings namely:

$$I) \quad \alpha_p = 0 \quad \phi_p = 0$$

$$\text{III)} \quad \alpha_p = \alpha_{p\text{III}} \quad \phi_p = 0$$

$$\text{IV)} \quad \alpha_p = \alpha_{p\text{IV}} \quad \phi_p = 0$$

and the B probe is used in a fixed position, namely:

$$\text{II)} \quad \alpha_p = 0 \quad \phi_p = \phi_{p\text{II}}$$

For this case the topography of the calibration surfaces will appear as four hills. The three with their peaks at points $(0,0)$; $(+\alpha_{p\text{III}}, 0)$ and $(-\alpha_{p\text{IV}}, 0)$ are the translated hills $C_{p\text{rpA}}$ and the fourth with its peak at $(0, \phi_{p\text{II}})$ is the translated hill $C_{p\text{rpB}}$. Their contours of constant C_p are then as shown in figure 4.

Assume now that a velocity vector with yaw α and pitch ϕ is to be measured. These values of α and ϕ will be sensed uniquely by the probes at their four angular settings. Were equation (4) single valued, the values of α and ϕ could be uniquely evaluated, as the single intersection point between the projections of appropriate lines of constant C_p on the α, ϕ plane*. In the present case of the double valued functions, the lines of constant C_p are closed curves and more than a single intersection point do exist.

* C_p has generally a different value for each probe in each of its settings. Thus the solution involves solving for the intersection points between projections of contours of specified (but different) C_p values on the different hills.

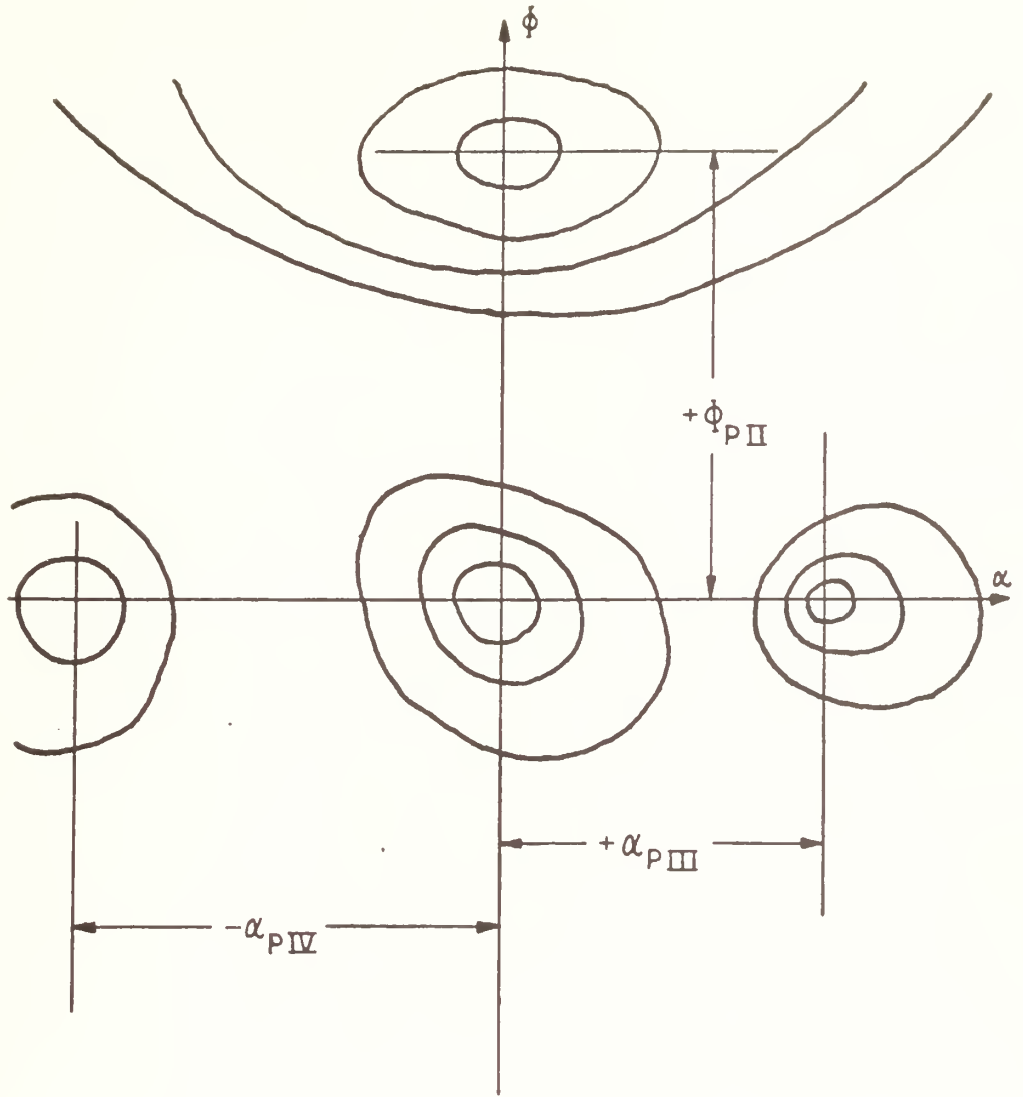


Fig. 4: Projections of $C_p = \text{const.}$ lines of the four calibration surfaces (the center hill is for probe A at $\alpha_p = 0$, $\phi_p = 0$, the top hill is for probe B at $\alpha_p = 0$, $\phi_p = \phi_{pII}$, the right hill is for probe A at $\alpha_p = +\alpha_{pIII}$, $\phi_p = 0$ and the left hill is for probe A at $\alpha_p = \alpha_{pIV}$, $\phi_p = 0$).

The situation is shown in Fig. 5 for an example of a number of such intersection points. The correct intersection point, however, is uniquely identified as the only point through which all four $C_p = \text{const.}$ curves pass.

From an examination of Fig. 5 it is clear that the intersection points of three closed C_p curves projections only are sufficient to identify α and ϕ uniquely. However one of these three curves must be that belonging to the type B probe.

The details of the numerical procedure used to obtain the correct intersection point in the evaluation of α and ϕ , are given in the following paragraph.

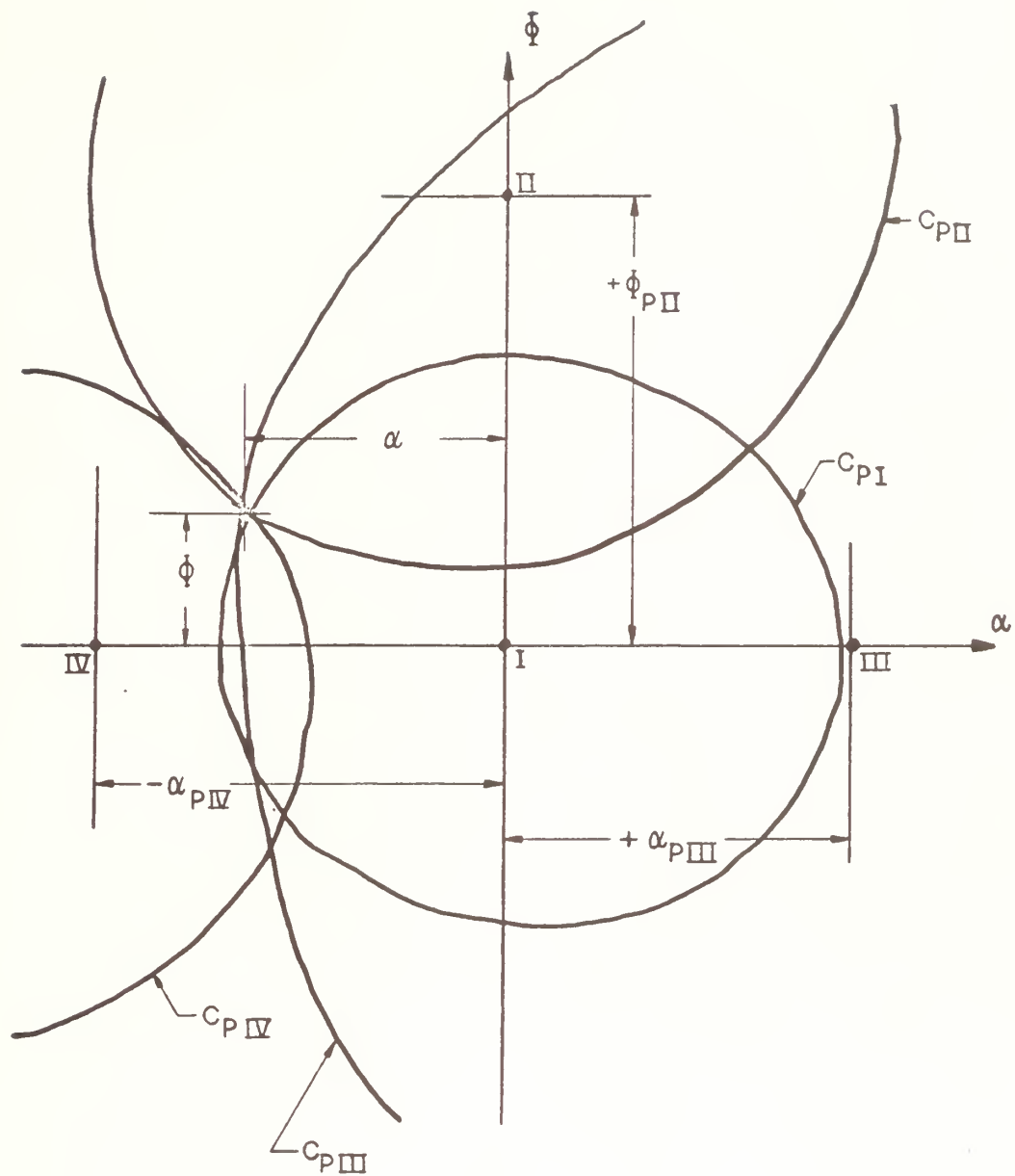


Fig. 5: An example showing a number of intersection points. The real one is in the second quadrant.

Evaluation of the intersection point coordinates (numerical Procedure)

The calibration surfaces Cp_{rp} are represented in form of a linear string of values ordered into an array, as shown schematically in figure 6. The numbers in Fig. 6 indicate the position of a Cp_{rp} value in the string. The string starts with the value of Cp_{rp} at a point $(-\alpha_{rpLo}; -\phi_{rpLo})$ and ends with the value of Cp_{rp} at a point $(+\alpha_{rpUp}; +\phi_{rpUp})$. This sequence must be kept and can not be changed.

Each of the closed $Cp = \text{const.}$ curves projections in figs. 2 and 3 is the projection of the line of intersection between a plane parallel to the α, ϕ plane at a height equal to Cp and the calibration surface. These closed curves can be determined as the locus of the projections of all the penetration points of arbitrary lines parallel to the α, ϕ plane at a height Cp and the calibration surface. Such penetration points are calculated in subroutine "PENPTS", Fig. 10.

PENPTS calculates the first two penetration points of a surface Z (in the present case $Z = Cp$) by a straight line piercing that surface. If the surface is double valued these two points are the only roots. The surface is given as a table of numbers on a cartesian basis $Z = Z(X, Y)$ (or in the present case $Cp = Cp(\alpha, \phi)$).

The subroutine has the following limitations:

- 1) No roots can be found on the lower $Y = \text{const.}$ boundary

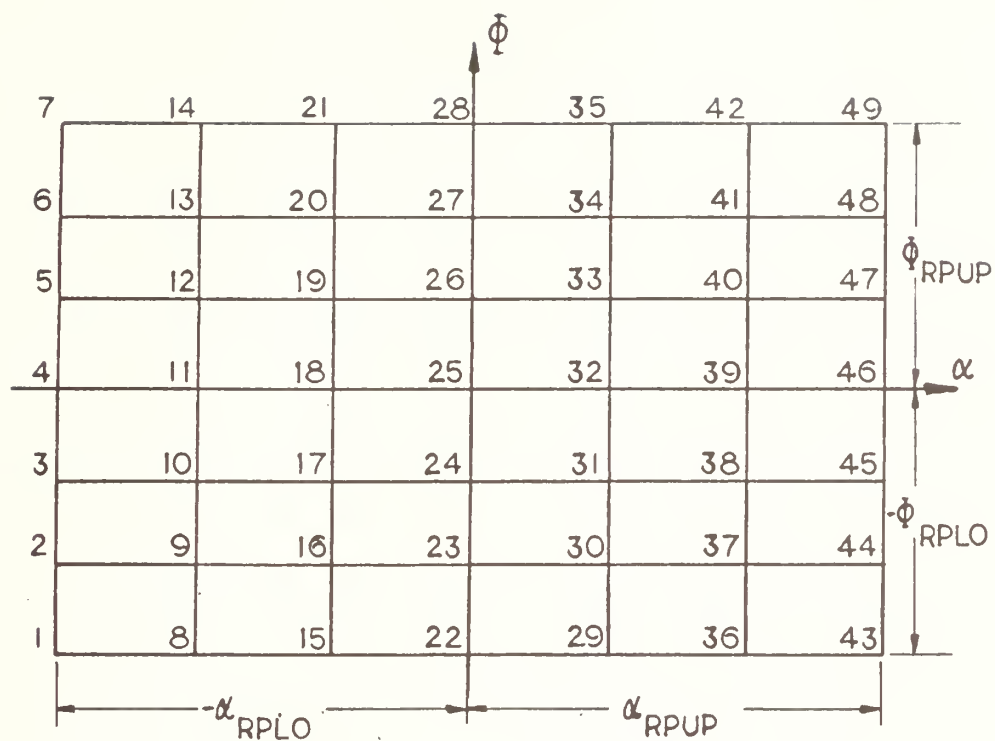


Fig. 6: The order of a calibration surface array.

- 2) The roots can be found only along a piercing line which is parallel to the X axis (but at any height above the X,Y plane)
- 3) The table $Z = Z(X,Y)$ defining the surface must be based on a grid comprising lines $X = \text{const.}$ and $Y = \text{const.}$ The spacing of these lines must not be equal. In other words the surface is defined by a rectangular grid in the X,Y plane, from X_{\min} to X_{\max} and from Y_{\min} to Y_{\max} .
- 4) Only a single root can be evaluated in a surface element located above a defining rectangle on the X,Y plane.
- 5) Not more than the first two roots will be evaluated for any piercing line.
- 6) The surface must be monotonic over each rectangle (this is a result of limitation 4).
- 7) All X and Y arguments must be given in increasing order.

These limitations do not restrict the application of PENPTS in the present problem as long as the calibration surfaces are smooth within the element located above a grid rectangle. However, the elemental grid rectangles can be reduced arbitrarily in size. If a calibration surface is more than double valued PENPTS will fail. However in this case the probe yielding such a calibration surface can not be considered a useful instrument unless used only in parts of the domain where it is double valued.

Z is defined from X_{\min} to X_{\max} and from Y_{\min} to Y_{\max} . PENPTS is given the following initial information: X values and Y values defining grid points, corresponding Z values, the Y location (YG) and the height above the X,Y plane (HT) of the piercing line. With this information PENPTS searches for the band of rectangles which includes YG or of which YG is the lower boundary (see fig. 7) and then scans this band from left to right in search for penetration points. The scanning is based on the geometry given in fig. 7 which represents a particular element in the band, approximated by two plane triangles.

Initially a coarse scan is carried out just to detect, but not to evaluate, an intersection point. This is done checking for each sub-domain whether $(ZX(I-1) - HT)/(ZX(I) - HT) \leq 0$. If this condition is true a root is detected and control is transferred to its exact evaluation. The value of the root is calculated after its location, either in the first (left) or second (right) triangle is determined (each grid rectangle is composed of two triangles). Equation 6 which is based on fig. 8 (for a left triangle) or eq. 7 which is based on fig. 9 (for a right triangle) is used to evaluate the penetration point. These equations express the linear interpolation of C_p in the Fortran rotation used in this program.

$$XS = X(I-1) + \frac{ABS(ZX(I-1)-HT)*(XM-X(I-1))}{(ABS(HT-ZM) + ABS(ZX(I-1)-HT))} \quad (6)$$

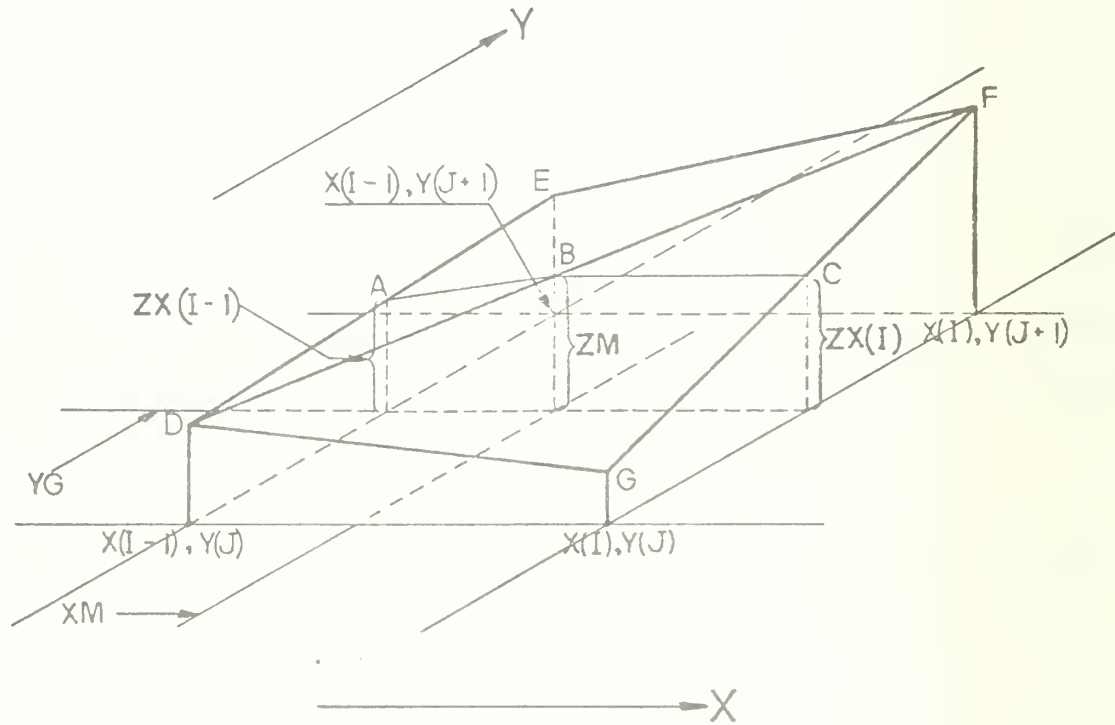


Fig. 7: The geometry of a linearized calibration surface element comprising two plane triangles and its intersection with a plane normal to X, Y along $Y = Y_G$.

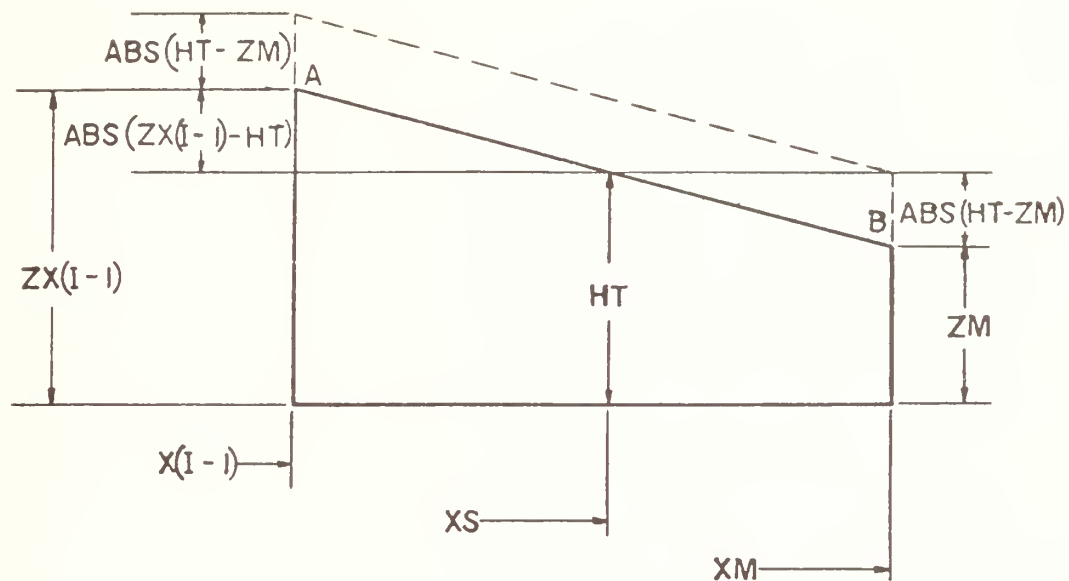


Fig. 8: The geometry for a penetration through a left hand (first) triangle.

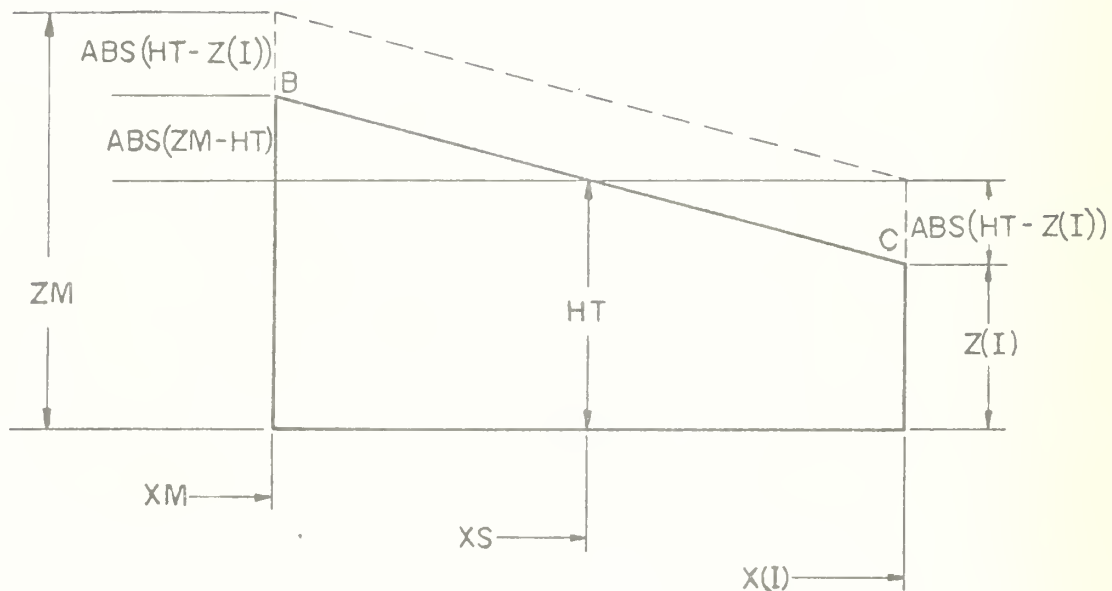


Fig. 9: The geometry for a penetration through a right hand (second) triangle.

$$XS = XM + (X(I) - XM) * ABS(ZM - HT) / (ABS(ZM - HT) + ABS(HT - Z(I))) \quad (7)$$

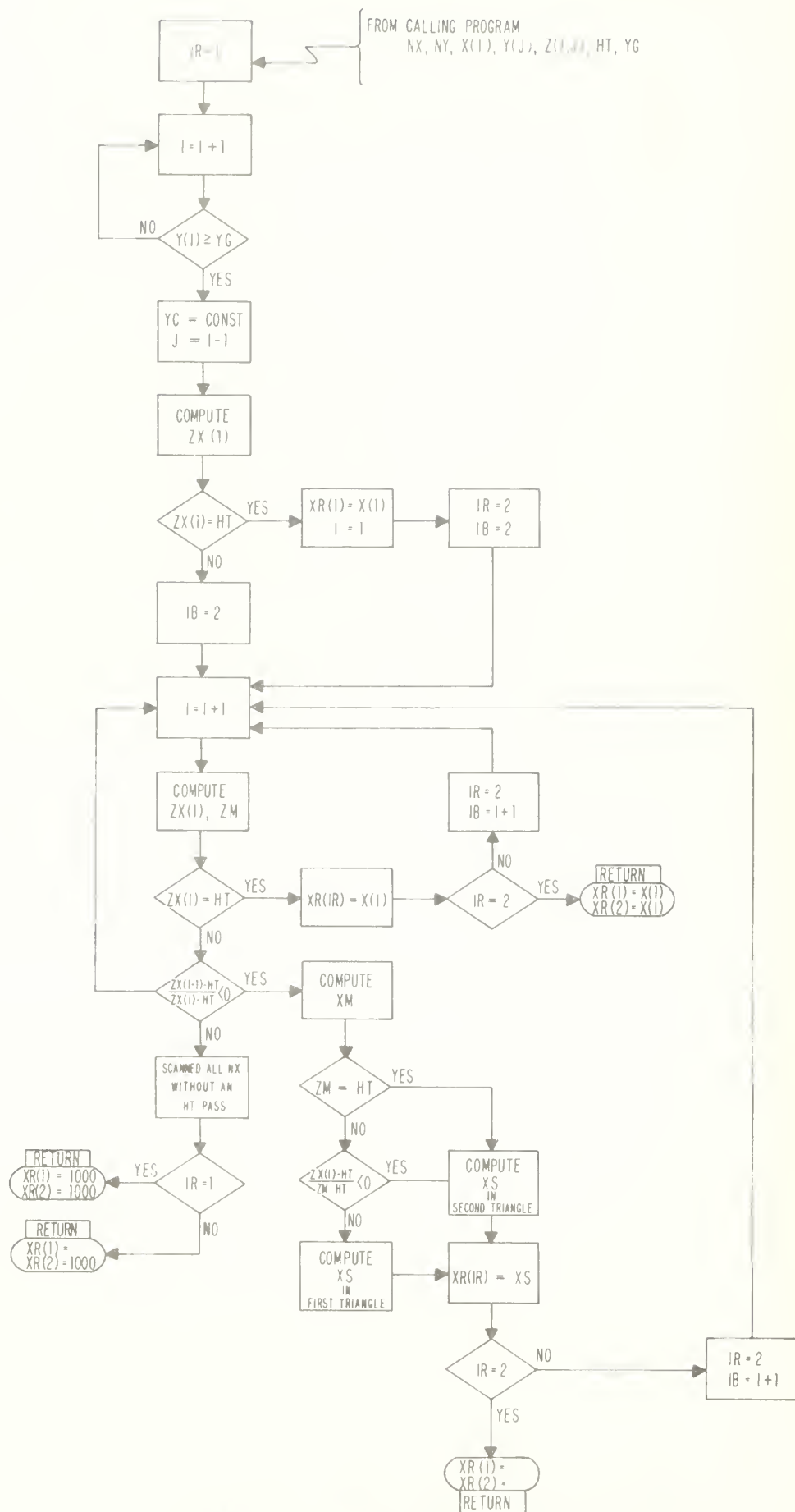
Equations 6 and 7 are invariant to the slope of the calibration surface i.e., the slope of the straight lines AB and BC.

Finally it should be pointed out that when two penetration points are determined the values of their abscissas, $X(I)$, are returned. When only a single penetration point is detected the abscissa $X(2)$ will be returned with a value of 1000.0. When no penetration point is determined both $X(I)$ values returned will have the value of 1000.0. The program logic is designed to recognize these messages.

It was stated earlier that PENPTS is used to determine the closed intersection curves projections on the X,Y plane. In fact not the curves but just the intersection points between each two of them are required (see figure 3).

To compute the coordinates of these points the subroutine "INTSCS" is used. It uses PENPTS as a subroutine.

In INTSCS a scanning procedure is carried out from a minimal value of Y (or ϕ) $YRIN$ to an upper value of $YRUP$, or a



prescribed 10,000 times* which ever comes earlier. The sub-routine scans through any two arbitrarily chosen closed curve projections to find their intersection points. In each scan (I) up to four penetration points can be determined, while the penetration points of the previous scan (J) are memorized. Together, eight penetration points can be involved. When no intersection point exists the geometrical situation is as shown in figure 11, while the existence of an intersection point is characterized in figure 12. Subroutine INTSCS can distinguish between the two situations. In figures 11 and 12 the case of four penetration points found in each scan are shown. The subroutine, however will handle any possible number of such points, from zero to four. A "no penetration points" is assigned an abscissa value of 1000.0 by PENPTS as explained earlier.

When an intersection point is detected its evaluation is based on the geometry shown in fig. 12. The eight penetration points have the following coordinates:

AJL(RAJL,YRJ)	BJL(RBJL,YRJ)
BJR(RBJR,YRJ)	AJR(RAJR,YRJ)
BIL(RBIL,YR)	AIL(RAIL,YR)
AIR(RAIR,YR)	BIR(RBIR,YR)

* The 10,000 scans are governed by a program constant in the line "DO 140" and can be arbitrarily varied.

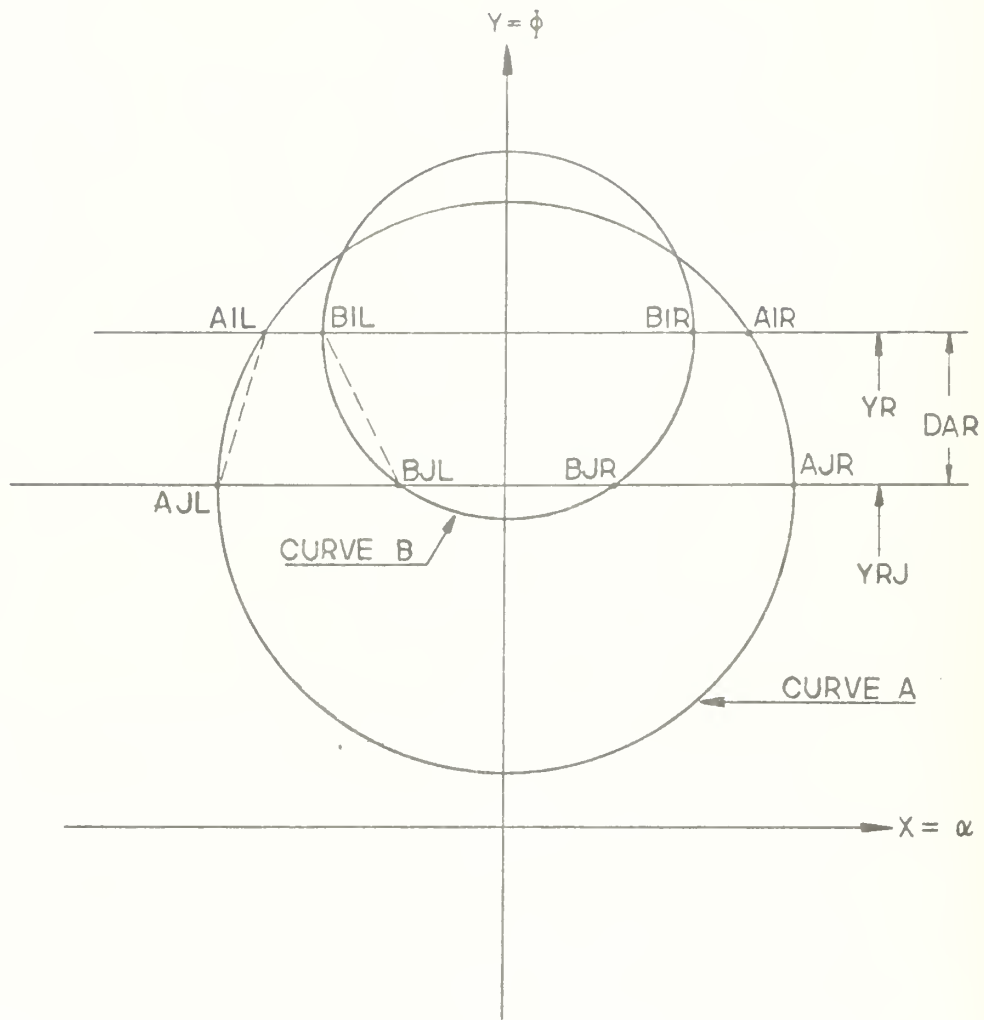


Fig. 11: The geometry for two successive scans when no intersection point exists.

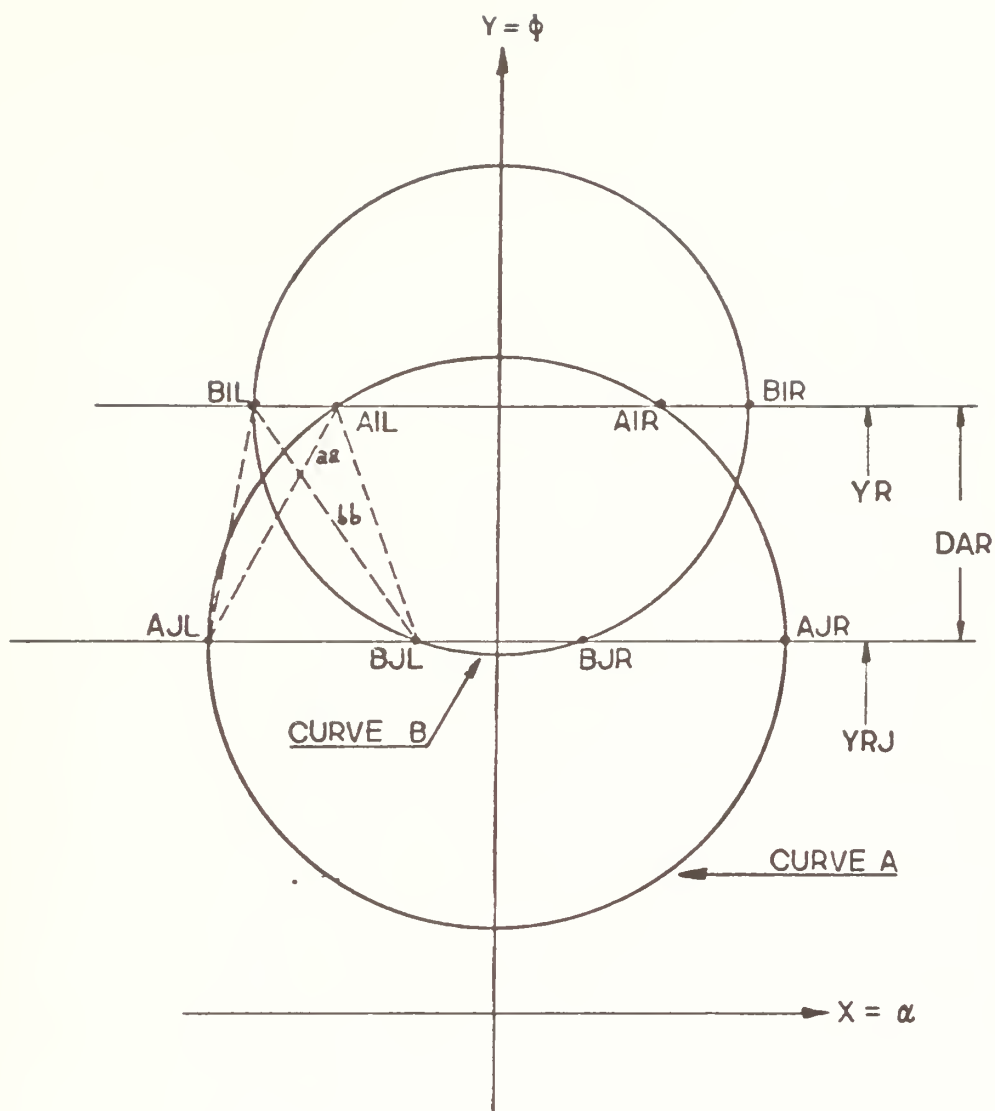


Fig. 12: The geometry for two successive scans when an intersection point does exist.

The left intersection point illustrated in fig. 12 is the intersection point of the lines aa and bb, each described by its equation:

$$\text{for aa } Y = (AA)X + BA \quad (8)$$

$$\text{for bb } Y = (AB)X + BB \quad (9)$$

The constants AA, BA, AB and BB are given in equations 10 to 13.

$$AA = (YRJ - YR) / (RAJL - RAIL) \quad (10)$$

$$BA = YR - AA * RAIL \quad (11)$$

$$AB = (YRJ - YR) / (RBJL - RBIL) \quad (12)$$

$$BB = YR - AB * RBIL \quad (13)$$

The coordinates of the intersection point to be calculated are

$$X = (BB - BA) / (AA - AB) \quad (14)$$

$$Y = X * AA + BA \quad (15)$$

These relations are true for a left hand intersection point.

Analogous equations are true for a right hand intersection point. In this algorithm the straight lines aa and bb approximate the curved lines connecting AJL with AIL and BJL with BIL or similar lines on the right hand side of figure 12. The error introduced through this approximation is reduced as $DAR = \Delta\phi$ is reduced.

It is possible that an intersection point is identical with AIL and BIL or AIR and BIR. This case is defined as "direct hit". The program is designed to detect such a direct hit and evaluate the corresponding intersection point accordingly.

The above algorithm works perfectly as long as the two closed $C_p = \text{const.}$ curves are far from being tangent. But in

practice a situation of almost tangent curves can arise when X (or α) is very small. In this case the preceeding algorithm will fail and must be replaced. The geometry of this situation is described in figure 13. This situation is identified by INTSCS and the intersection points are then evaluated assuming that they are intersections of two circular arcs. When the curves $C_p = \text{const.}$ are almost circular this approximation does not lead to unacceptable errors.

It was stated earlier that INTSCS scans from a minimum value of ϕ to a maximum value of ϕ with prescribed steps $\Delta\phi$, as shown in figs. 11 and 12. This direction of the scanning is used when the intersection points of the curves C_{p_I} and $C_{p_{II}}$ of fig. 5 are evaluated.

However, in course of the reduction of the measured data, scans in the direction of α in steps of $\Delta\alpha$ are also necessary to evaluate the intersections of the curves C_{p_I} and $C_{p_{III}}$ or C_{p_I} and $C_{p_{IV}}$. INTSCS is designed to carry out this task as well. To do this the calling statement for INTSCS is appropriately changed as will be explained in the next section. To be general enough INTSCS is not written in terms of α and ϕ or X and Y but rather in terms of general arguments. The best way to understand INTSCS is to compare its general arguments to physical quantities by means of the calling statements. In fig. 14 the flow diagram in INTSCS is given in terms of the general arguments.

INTSCS returns to the main program (fig. 15) the (α, ϕ) coordinates of two intersection points between the $C_p = \text{const.}$ curves specified in the calling statement. Let us now follow the way in which the main program is designed to utilize INTSCS

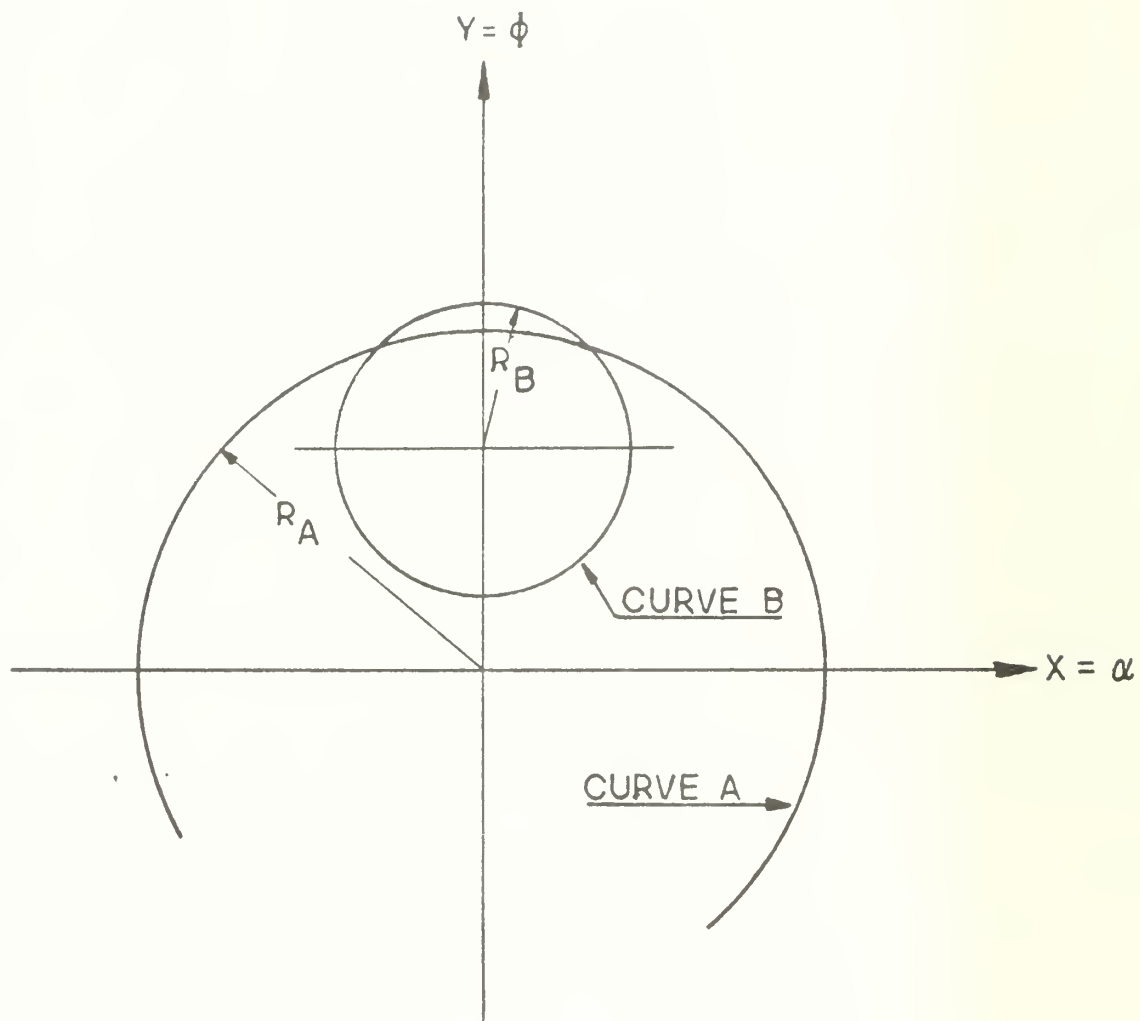


Fig. 13: The geometry when two closed $C_p = \text{const.}$ curves are almost tangent.

for the evaluation of α and ϕ of the velocity vector, as well as static and total pressures.

Evaluation of the Velocity Vector and Pressures from the Probe Signals

Fortran program VDR was written to evaluate the velocity vector from probe measurements of pressures. The program is shown in Fig. 15.

At line 1410 INTSCS is called to scan curves I and II for possible intersection points. Scanning can be carried out in the direction of the ordinate only, with the calibration curve matrices compiled exactly as shown in fig. 6. This limitation is imposed by the way PENPTS is constructed. In the case of the intersection points between I and II ZA and ZB are scanned without difficulties in the direction of the ordinate which is ϕ as shown in fig. 12 and returns with the coordinates of the two first intersection points, points 1 and 2 of Fig. 16. They are ALF1, PHI1 and ALF2, PHI2. In line 1500 INTSCS is called again to scan curves I and III. Now scanning has to be carried out in the direction of the abscissa, a task for which INTSCS was not designed. To overcome this problem the calibration curve matrices are used in a transformed form such that the previous abscissas are now ordinates, ordinates are abscissas and the internal structures of the Cp_{rp} arrays are accordingly modified. This transformation is carried in VDR in the section between lines 320 and 450. Comparison of the calling line 1500 to the previous calling line 1410 shows very clearly how the various arrays: original and transformed, are used. The coordinates of points 3 and 4 of fig. 16

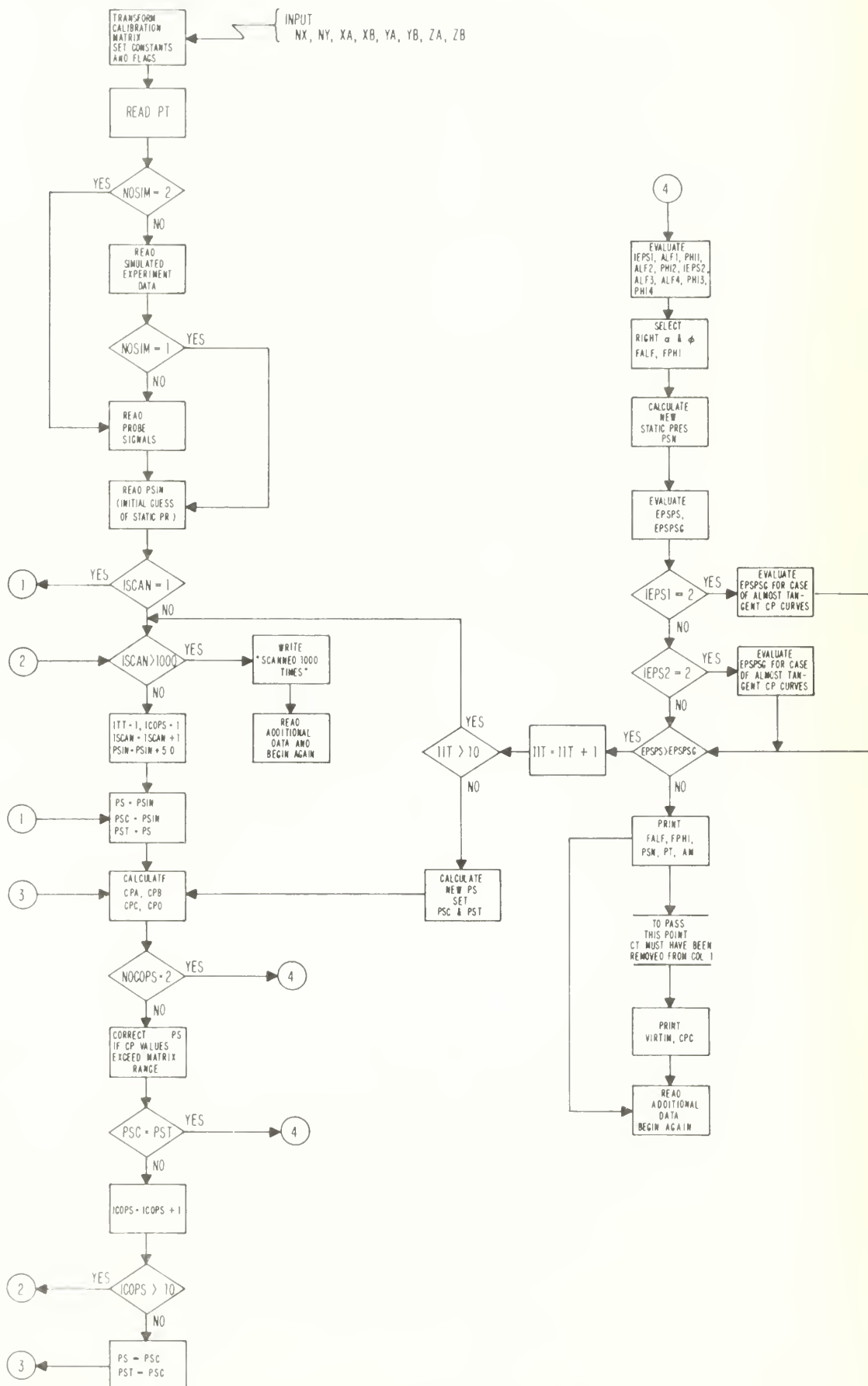


FIGURE 15. FLOW DIAGRAM OF VDR

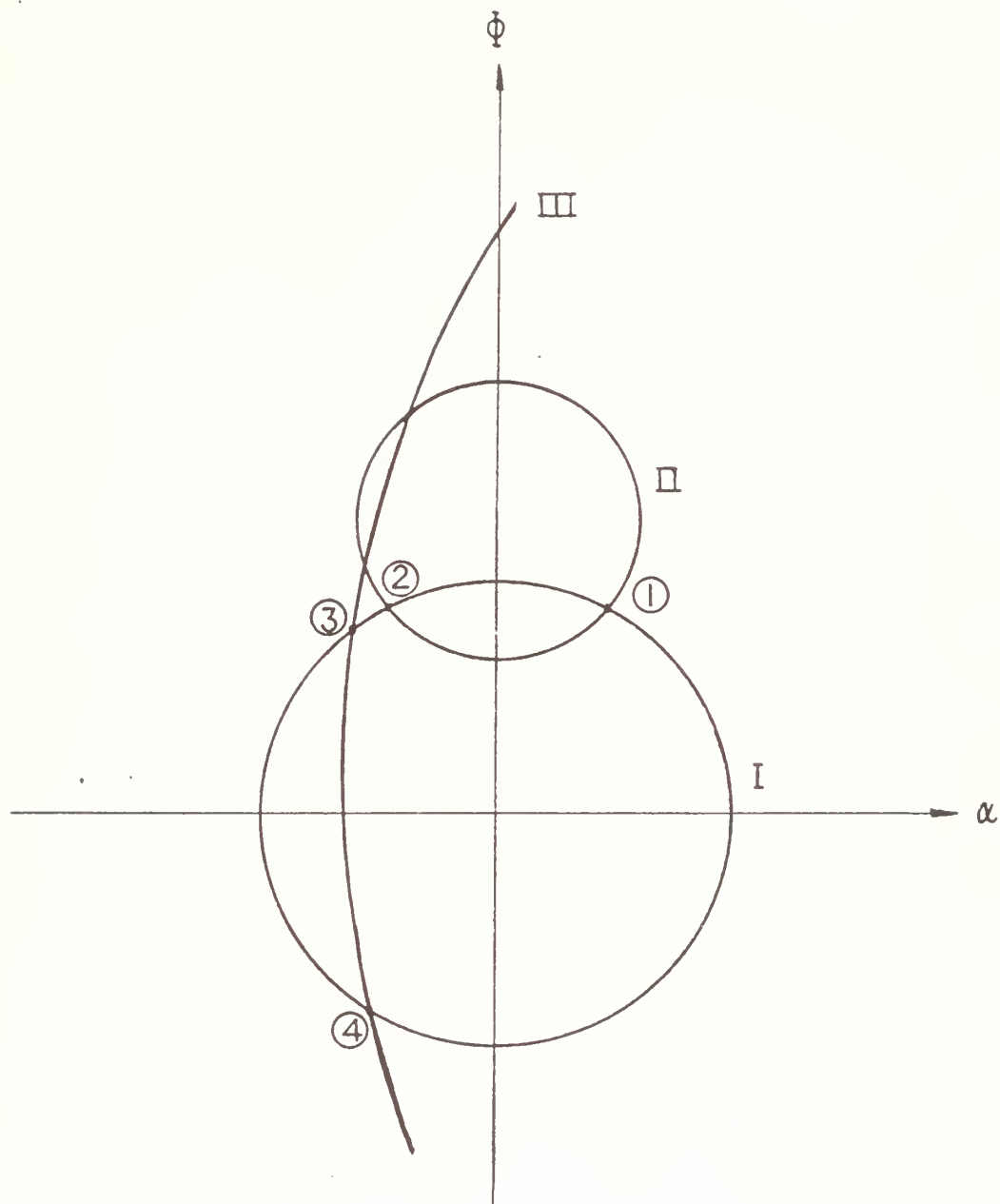


Fig. 16: Selection of the proper intersection point in VDR.

are now returned to the main program of VDR, they are ALF3,PHI3 and ALF4,PHI4.

We are seeking a single intersection point; the one representing yaw and pitch as sensed by probe A in positions I and III and probe B in position II. But, as the calibration surfaces are double valued we are now, unfortunately, in the possession of four points. The solution, however, is physically unique. Only a single velocity vector exists in reality and its yaw and pitch are included in the four intersection points evaluated. Were both the measurements and the numerical procedure absolutely accurate, two of the four points would have been identical. But this is not the case in reality, instead of a single point, two points close to each other will be detected. Therefore the average coordinates of the two of the four intersection points returned to VDR from INTSCS which are closest to each other are selected as the measured yaw and pitch angles. In the example shown in fig. 16 this will be the point dividing the distance between points 2 and 3.

The calculation is now at the point at which α and ϕ are temporarily known (see fig. 3). Using α and ϕ a new Cp_{rpIV} (for probe A in position IV) is computed by linear interpolation using subroutine INTPLT. With this new value of Cp_{rpIV} and with Pp_{IV} a new P_s is computed. If this new value of P_s is close enough as determined by EPSPSG to the guessed value, or to the value of P_s in the previous iteration, the data reduction for the particular point in question is terminated.

The relative difference between present and previous P_s is compared to the convergence criterion EPSPSG. This criterion is evaluated by an empirical function determined to give best compromise between accuracy of results and computer time required until convergence is achieved. When the calculation follows normal routine the convergence criterion is given in line 1710 as function of P_T . When the routine for almost tangent curves is used during data reduction either on the right or the left side a different empirical function (lines 1720 or 1730) is used.

If the convergence criterion is satisfied results are printed out and data for a new measurement point is read for reduction. If, however convergence is not reached a new static pressure for a next iteration is evaluated (line 1780).

Convergence and accuracy

The convergence of the present iterative procedure is not ensured in all possible cases of data sets. The program, however, is adjusted to converge in most of the cases. Similarly to other iterative computation method some experience is required to achieve convergence when the calculation does not converge. In this paragraph the principal factors affecting convergence, computation time and accuracy, which are obviously coupled, are pointed out.

The convergence and accuracy of reduction of a data set: P_T , PPA, PPB, PPC, PPD, PSIN (or analogous set in the experiment simulation mode) depends on the following factors, which can be varied by the user.

- 1) Coarseness of calibration arrays ZA, ZB and their linearity. With coarser arrays convergence problem will increase and accuracy of results decrease.
- 2) Probe settings YPB, XPC, XPD (with the following probe settings being fixed and not variable $YPA = YPC = YPD = 0.0$; $XPA = XPB = 0.0$). The optimum setting is about $\pm 20^\circ$ to 25° . Too small values reduce accuracy, too big values cause convergence problems and probe tip flow separation.
- 3) RELXPS, the static pressure relaxation factor. The smaller this factor the safer will convergence be achieved. Computation time, however, will increase.
- 4) The constant 5.0 in line 1050 of the program. The dimension of this constant is kg/m^2 . If too big results can be lost and if too small computer time will be growing. The variation of this constant should be coupled with an appropriate modification of the constant in line 1010 of VDR (item 8 in this list).

- 5) The constants in the evaluation of EPSPSG (lines 1710 to 1730). The smaller EPSPSG the more accurate the results in expense of increased computation time and reduced convergence safety.
- 6) The constant scanning step DAR. The smaller DAR the more accurate the results, but too small values can cause complete loss of results. Computation time increases with reduced DAR.
- 7) The constant 10 in line 1360. This constant governs the number of P_s corrections.
- 8) The constant 1000 in line 1010. This constant governs the number of scans.

If convergence is not achieved in a particular case variation of each or of a combination of the above values will always enable convergence.

Evaluation of the Computation Time

By deleting the letters CT from column 1 and 2 of lines 20 to 70, 1930 to 1960, 1980, 2000, 2010 the actual computation time as well as CPU time are evaluated and printed out. The following statement prior to execution is required in this case:*

GLOBAL T SYSLIB SSPLIB

This option is useful for adjusting the constants affecting convergence as to optimal compromise between accuracy, ease of convergence and calculation costs.

* When the program is run on Naval Postgraduate School IBM 360 system.

Input

- 1) Calibration arrays have to be input in the following manner: first values of NX and NNY , second values of X in rising order, third values of Y in rising order and fourth values of Z in the order shown in Fig. 6. Two calibration arrays are read: first the array of type A probe and second the array of type B probe.
- 2) If the program is run in experiment simulation mode PT and PS are read in Kg/m^2 and subsequently ϕ and ϕ .
- 3) If the program is run in data reduction mode the measured values of PT , PPA , PPB , PPC and PPD are read and then the guess of static pressure $PSIN$. All are read in Kg/m^2 . $PSIN$ has to be lower than the actually existing value to ensure convergence of the calculation. Too low a value will cause waste of computer time.

Calibration arrays are read from a disk space on which they are stored. The following statement prior to execution is required for successful reading:

```
FILEDEF 02 DSK NAME XX
```

here NAME is the name of the file on which the calibration data of probes A and B is stored in proper order and format, XX is a two digit number.

Simulation or measurements reduction input is read in the normal way using the terminal keyboard or punched cards.

Output

α , ϕ , P_S , P_T and Ma are printed out according to lines 1820 to 1920. This output, however is not sufficient when the logic of the computation is to be followed either to examine the execution of the program or for debugging. Two programs with additional output are given in appendices 2 and 3 and can be used for this purpose. The first, SWVDR gives short additional output, namely:

- 1) When PSIN is successively increased automatically by the program to ensure convergence, the values of PSIN are printed out.
- 2) IIT, FALF, FPHI and PSN are printed out at the end of each iteration prior to the convergence test.

The second program WVDR prints more detailed information. All additional WRITE statements in this program are numbered with three digit numbers starting with 9.

Conclusions

The following conclusions are drawn on the basis of experience gained in running the program with various data sets and various types of calibration surfaces.

- 1) Optimal probe settings for ease of convergence and high accuracy are: $YPB = 250$, $XPC = 250$, $XPD = -250$. It is therefore suggested that a B type probe with 250 pitch will be used, and that the A type probe be rotated to ± 250 .
- 2) Convergence and accuracy, as well as computer time efficiency are improved when the calibration surfaces of both probes are not flat at their peaks but are rather rounded. It is therefore suggested that a new probe tip geometry be considered. A spherical tip with a central pressure tap is recommended. To prevent damage to the sensitive transducer located behind the pressure tap, and in order to improve the frequency response of the probes it is suggested that the volume between the pressure tap face and the transducer be filled with an appropriate liquid that will not affect the transducer negatively. In this case the opening of the pressure tap has to be sealed with a very thin low inertia membrane.
- 3) It is probably possible to modify the iterative procedure such that safe convergence can be achieved also when using the scheme of Fig. 2. If this can be achieved the Kiel probe will not be necessary. An effort in this direction is suggested.

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2. Shreeve, P. P., Simmons J. M., Winters K. A., and West J. C. Jr. "Determination of Transonic Compressor Flow Field by Synchronized Sampling of Stationary Fast Response Transducers", Symposium on Non-Steady Fluid Dynamics, ASME 1978 Winter Annual Meeting, San Francisco, Dec 1978. (To be published in ASME Journal of Fluids Engineering)
3. Thompkins W. T. Jr., and Kerrebrock J. L., "Exit Flow From a Transonic Compressor Rotor", AGARD Conference Proceedings No. 177, Unsteady Phenomena in Turbomachinery, pp. 6-1 to 6-23. Meeting held at Naval Postgraduate School, Monterey, California, 22-26 September 1975.
4. Shreeve R. P., McGuire A. G., and Hammer J. A., "Calibration of a Two Probe Synchronized Sampling Technique for Measuring Flows Behind Rotors", paper to be presented at IEEE, Eighth International Congress in Instrumentation in Aerospace Simulation Facilities, Naval Postgraduate School, Monterey, September 24-26 1979. Published as IEEE ICIAF Record of Proceedings.

APPENDIX I

LISTING OF VDR

07/08/79 18.43.34

FILE: VDR FORTRAN P1

N

P

S

```

C START OF VDR
CT INTEGRAL A(6)
CT IASC=0
CT IASC=0
DIMENSION ALF(10),PHI(10),XA(40),YA(40),
1ZA(40,40),XE(40),YE(40),ZS(40,40),XAX(40),YAX(40),
2ZAX(40,40),XBX(40),YBX(40),ZBX(40,40)
119 FORMAT(215)
131 FORNAT(F7.1)
130 FORNAT(F5.1)
120 FORNAT(F8.3)
132 FORNAT(F10.3)
135 FORNAT(F15.5)
136 FORNAT(F17.5)
C READ PROBE CALIBRATION DATA
READ(2,119) IX,NY
DO 121 I=1,NX
121 READ(2,130) XA(I)
DO 122 I=1,NY
122 READ(2,130) YA(I)
DO 123 I=1,NX
DO 123 J=1,NY
123 READ(2,120) ZA(I,J)
DO 221 I=1,NX
221 READ(2,130) XE(I)
DO 222 I=1,NY
222 READ(2,130) YE(I)
DO 223 I=1,NX
DO 223 J=1,NY
223 READ(2,120) ZS(I,J)
C TRANSFORM CALIBRATION MATRICES
DO 224 I=1,NY
224 XAX(I)=XA(I)
DO 225 I=1,NX
225 YAX(I)=YA(I)
DO 226 I=1,NY
DO 226 J=1,NX
226 ZAX(I,J)=ZA(J,I)
DO 227 I=1,NY
227 XBX(I)=XE(I)
DO 228 I=1,NX
228 YBX(I)=YE(I)
DO 229 I=1,NY
DO 229 J=1,NX
229 ZBX(I,J)=ZS(J,I)
C PROBE SETTINGS
YPA=C.C
YPE=55.
XPA=0.0
XPC=20.
XPL=-20.
C PROGRAM CONSTANTS
YRLD=-30.
YRLP=30.
YRLN=-30.
XRLD=-30.
XRLP=30.
XRLN=-30.
ICCP=1
NOCOP=1
NOSIM=1
IIT=1
ISCAN=1
RELXPS=0.5
C EXPERIMENT SIMULATION
401 FORMAT(F15.4)
193 READ(5,401) PT
WRITE(6,401) PT
IF(NOSIM.EQ.2) GO TO 500
READ(5,401) PS

```

```

INT00010
INT00020
INT00030
INT00040
INT00050
INT00060
INT00070
INT00080
INT00090
INT00100
INT00110
INT00120
INT00130
INT00140
INT00150
INT00160
INT00170
INT00180
INT00190
INT00200
INT00210
INT00220
INT00230
INT00240
INT00250
INT00260
INT00270
INT00280
INT00290
INT00300
INT00310
INT00320
INT00330
INT00340
INT00350
INT00360
INT00370
INT00380
INT00390
INT00400
INT00410
INT00420
INT00430
INT00440
INT00450
INT00460
INT00470
INT00480
INT00490
INT00500
INT00510
INT00520
INT00530
INT00540
INT00550
INT00560
INT00570
INT00580
INT00590
INT00600
INT00610
INT00620
INT00630
INT00640
INT00650
INT00660
INT00670
INT00680
INT00690
INT00700

```



```

WRITE(6,401) PS
READ(5,401) ALFA
WRITE(6,401) ALFA
READ(5,401) PHII
WRITE(6,401) PHII
CALL INITPLT(XA,YA,ZA,ALFA,PHII,NX,NY,CPA)
ALFC=ALFA-APC
CALL INITPLT(XA,YA,ZA,ALFC,PHII,NX,NY,CPC)
ALFD=ALFA-APD
CALL INITPLT(XA,YA,ZA,ALFD,PHII,NX,NY,CPD)
PHIB=PHII-YPB
CALL INITPLT(XB,YB,ZB,ALFA,PHIB,NX,NY,CPB)
FDYN=PT-PS
PPA=CPA*POYN+PS
PPB=CPB*POYN+PS
PPC=CPC*POYN+PS
PPD=CPD*POYN+PS
C READ MEASUREMENTS DATA
IF(ISCAN.EQ.1) GO TO 501
500 READ(5,135) PPA
WRITE(6,135) PPA
READ(5,135) PPB
WRITE(6,135) PPB
READ(5,135) PPC
WRITE(6,135) PPC
READ(5,135) PPD
WRITE(6,135) PPD
501 READ(5,135) PSIN
WRITE(6,135) PSIN
IF(ISCAN.EQ.1) GO TO 181
180 IF(ISCAN.GT.1000) GO TO 305
IIT=1
ICUPS=1
ISCAN=ISCAN+1
PSIN=PSIN+5.0
181 PS=PSIN
PSC=PSIN
PST=PS
C CALCULATES PRESSURE COEFFICIENTS
300 POYN=PT-PS
CPA=(PPA-PS)/POYN
CPB=(PPB-PS)/POYN
CPC=(PPC-PS)/POYN
CPD=(PPD-PS)/POYN
C CORRECTS PS ASSUMPTION TO ENSURE CP ARE IN CALIBRATION RANGE
IF(NOCIPS.EQ.2) GO TO 301
ZAMAX=-10000.
CALL MAXARY(ZA,ZAMAX,NX,NY)
IF(CPA.GT.ZAMAX) PSC=1.01*PS
IF(CPB.GT.ZAMAX) PSC=1.01*PS
IF(CPD.GT.ZAMAX) PSC=1.01*PS
ZEMAX=-10000.
CALL MAXARY(ZB,ZEMAX,NX,NY)
IF(CPB.GT.ZBMAX) PSC=1.01*PS
ZAMIN=10000.
CALL MINARY(ZA,ZAMIN,NX,NY)
IF(CPA.LT.ZAMIN) PSC=0.99*PS
IF(CPC.LT.ZAMIN) PSC=0.99*PS
IF(CPD.LT.ZAMIN) PSC=0.99*PS
ZBMIN=10000.
CALL MINARY(ZB,ZBMIN,NX,NY)
IF(CPB.LT.ZBMIN) PSC=0.99*PS
IF(PSC.EQ.PST) GO TO 301
ICUPS=ICUPS+1
IF(ICUPS.GT.10) GO TO 180
PS=PSC
PST=PSC
GO TO 300
C CALCULATES TWO ALF & PHI ANGLES FOR 'I' & 'II'

```

```

INT00710
INT00720
INT00730
INT00740
INT00750
INT00760
INT00770
INT00780
INT00790
INT00800
INT00810
INT00820
INT00830
INT00840
INT00850
INT00860
INT00870
INT00880
INT00890
INT00900
INT00910
INT00920
INT00930
INT00940
INT00950
INT00960
INT00970
INT00980
INT00990
INT01000
INT01010
INT01020
INT01030
INT01040
INT01050
INT01070
INT01080
INT01090
INT01100
INT01110
INT01120
INT01130
INT01140
INT01150
INT01160
INT01170
INT01180
INT01190
INT01200
INT01210
INT01220
INT01230
INT01240
INT01250
INT01260
INT01270
INT01280
INT01290
INT01300
INT01310
INT01320
INT01330
INT01340
INT01350
INT01360
INT01370
INT01380
INT01390
INT01400

```

```

301 CALL INTSCS(YPA,YPB,YNLC,YFUP,YKIN,
1CPA,CPE,ALF,PHI,XA,YA,ZA,
2XB,YE,ZE,XAX,YAX,ZAX,XEX,YEX,ZEX,NX,NY,IEPS)
IEPS1=IEPS
ALF1=ALF(1)
ALF2=ALF(2)
PHI1=PHI(1)
PHI2=PHI(2)
C CALCULATES TWO ALF & PHI ANGLES FOR 'I' & 'III'
CALL INTSCS(XPA,XPC,XSLD,XRUP,XRIN,
1CPA,CPC,FH1,ALF,XAX,YAX,ZAX,
2XAX,YAX,ZAX,XA,YA,ZA,XA,YA,ZA,NX,NY,IEPS)
IEPS2=IEPS
ALF3=ALF(1)
ALF4=ALF(2)
PHI3=PHI(1)
PHI4=PHI(2)
C SELECTS THE PROPER ALF & PHI ANGLES OUT OF THE FOUR VALUES
HALF=(.5*(ALF1+ALF2+ALF3+ALF4)-AMAX1(ALF1,ALF2,ALF3,
1ALF4))-AMIN1(ALF1,ALF2,ALF3,ALF4))/2
FPHI=(.5*(PHI1+PHI2+PHI3+PHI4)-AMAX1(PHI1,PHI2,PHI3,PHI4)
1-AMIN1(PHI1,PHI2,PHI3,PHI4))/2
C CALCULATES IEPS FROM DATA OF POSITION IV
ALFCN=HALF-XPD
CALL INTFLT(XA,YA,ZA,ALFCN,FPH1,NX,NY,CPU)
ALFCN=HALF-XPC
CALL INTFLT(XA,YA,ZA,ALFCN,FPH1,NX,NY,CPC)
PSN=(PPC*CPU-PPD*CPC)/(CPU-CPC)
C CONVERGENCE TESTS
EPSPS=.13*(1-PSN-PS)/PS
EPSPCS=.00000000009*(PT**2.C)-.00000098*PT
IF(IEPS1.LT.2) EPSPS=.00000000009*(PT**2.C)-.00000098*PT
IF(IEPS2.EQ.2) EPSPS=.00000000009*(PT**2.C)-.00000098*PT
IF(EPSPS.GT.EPSPCS) GO TO 310
GO TO 303
310 IIT=IIT+1
IF(IIT.GT.10) GO TO 180
PS=PS+RELAPS*(PSN-PS)
FSC=PS
PST=PS
GO TO 300
303 WRITE(6,171) HALF
171 FFORMAT('0',' VELOCITY YAW IS' ,F15.2)
WRITE(6,172) FPHI
172 FFORMAT(' VELOCITY PITCH IS' ,F15.2)
WRITE(6,173) PSN
173 FFORMAT(' STATIC PRESSURE IS' ,F15.3)
WRITE(6,174) PF
174 FFORMAT(' TOTAL PRESSURE IS' ,F15.3)
AM=SQRT((PF/PSN)**0.285714-1.0)*5.0)
WRITE(6,175) AA
175 FFORMAT(' MACH NUMBER IS' ,F15.5)
CT CALL IXCLR(A)
CT VIRTIM=(A(5)-1A6)/76800
CT CPU=(A(6)-1A6)/76800
CT WRITE(6,450) VIRTIM
450 FFORMAT(' VIRTUAL TIME IS' ,F15.5)
CT WRITE(6,451) CPU
451 FFORMAT(' TOTAL CPU IS' ,F15.5)
CT 1A5C=A(5)
CT 1A6C=A(6)
GO TO 193
305 WRITE(6,307)
307 FFORMAT(' SCANNED 1000 TIMES')
GO TO 193
END
SUBROUTINE INTSCS(XR1,XR2,XRLD,XRUP,XRIN,
1HT1,HT2,RES1,RES2,X1,Y1,Z1,
2X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,N1,N2,IEPS)
DIMENSION RES1(10),RES2(10),ARCS(10),X1(40),Y1(40),
INT01410
INT01420
INT01430
INT01440
INT01450
INT01460
INT01470
INT01480
INT01490
INT01500
INT01510
INT01520
INT01530
INT01540
INT01550
INT01560
INT01570
INT01580
INT01590
INT01600
INT01610
INT01620
INT01630
INT01640
INT01650
INT01660
INT01670
INT01680
INT01690
INT01700
INT01710
INT01720
INT01730
INT01740
INT01750
INT01760
INT01770
INT01780
INT01790
INT01800
INT01810
INT01820
INT01830
INT01840
INT01850
INT01860
INT01870
INT01880
INT01890
INT01900
INT01910
INT01920
INT01930
INT01940
INT01950
INT01960
INT01970
INT01980
INT01990
INT02000
INT02010
INT02020
INT02030
INT02040
INT02050
INT02060
INT02070
INT02080
INT02090
INT02100

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```

121(40,40),X2(40),Y2(40),Z2(40,40),X3(40),Y3(40),
Z3(40,40),X4(40),Y4(40),Z4(40,40)
RES1(1)=9000.
RES1(2)=9000.
RES2(1)=9000.
RES2(2)=9000.
IEPS=1
IS1=1
ISP=1
CAP=1.
AR2R=AR1N
GO TO 152
AR2R=AR2R+CAP
AR2RJ=AR2R
152 ARM1=AR2R-ARP1
ARM2=AR2R-ARP2
C CHECK FOR LOWER CALIBRATION RANGE
IF (ARM1.LT.ARL1) GO TO 150
IF (ARM2.LT.ARL2) GO TO 150
K=1
C CALCULATES INITIAL PENETRATION POINTS
CALL PENPTS(N1,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJF=ARRES(2)
CALL PENPTS(N1,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBJL=ARRES(1)
RBJF=ARRES(2)
C CALCULATES SUCCESSIVE PENETRATION POINTS
DO 140 I=1,10000
AR2R=AR2R+CAP
ARM1=AR2R-ARP1
ARM2=AR2R-ARP2
C CHECK FOR UPPER CALIBRATION RANGE
IF (ARM1.GT.ARUP1) GO TO 195
IF (ARM2.GT.ARUP2) GO TO 195
CALL PENPTS(N1,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJF=ARRES(2)
CALL PENPTS(N1,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBJL=ARRES(1)
RBJF=ARRES(2)
IF (RAJL.EQ.1000.) ISL=10
IF (RAJF.EQ.1000.) ISF=10
IF (RBJL.EQ.1000.) ISR=10
IF (RBJF.EQ.1000.) ISF=10
IF (RAJL.EQ.1000.) ISL=10
IF (RAJF.EQ.1000.) ISF=10
IF (RBJL.EQ.1000.) ISR=10
IF (RBJF.EQ.1000.) ISF=10
C CHECK FOR DIRECT HIT ON LEFT INTERSECTION,EVALUATE IF REQUIRED
IF (ISL.NE.10) GO TO 164
ISL=1
GO TO 183
164 IF (RAJL.NE.RBIL) GO TO 180
RES1(K)=RBIL
RES2(K)=AR2R
IF (K.EQ.2) GO TO 155
K=2
GO TO 183
C CHECK FOR INTERMEDIATE LEFT INTERSECTION,EVALUATE IF REQUIRED
180 IF (ISL.NE.10) GO TO 160
ISL=1
GO TO 183
160 IF ((RAJL-RBIL)/(RAJL-RBIL).GT.C.0) GO TO 183
AA=(AR2R-AR2R)/(RAJL-RAJL)
BA=AR2R-AA*RAJL
AB=(AR2RJ-AR2RJ)/(RBJL-RBIL)
BB=AR2RJ-AB*RBIL
RES1(K)=(AA-AB)/(AA-AB)
RES2(K)=AA*RES1(K)+BA
INTC2110
INTC2120
INTC2130
INTC2140
INTC2150
INTC2160
INTC2170
INTC2180
INTC2190
INTC2200
INTC2210
INTC2220
INTC2230
INTC2240
INTC2250
INTC2260
INTC2270
INTC2280
INTC2290
INTC2300
INTC2310
INTC2320
INTC2330
INTC2340
INTC2350
INTC2360
INTC2370
INTC2380
INTC2390
INTC2400
INTC2410
INTC2420
INTC2430
INTC2440
INTC2450
INTC2460
INTC2470
INTC2480
INTC2490
INTC2500
INTC2510
INTC2520
INTC2530
INTC2540
INTC2550
INTC2560
INTC2570
INTC2580
INTC2590
INTC2600
INTC2610
INTC2620
INTC2630
INTC2640
INTC2650
INTC2660
INTC2670
INTC2680
INTC2690
INTC2700
INTC2710
INTC2720
INTC2730
INTC2740
INTC2750
INTC2760
INTC2770
INTC2780
INTC2790
INTC2800

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FILE: VDR FORTRAN 21 N P S

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      IF(K.EQ.2) GO TO 155
      K=2
C CHECK FOR DIRECT HIT OR RIGHT INTERSECTION, EVALUATE IF REQUIRED
183  IF (ISR.NE.10) GO TO 161
      ISR=1
      GO TO 163
161  IF (RAIR.NE.RBIR) GO TO 182
      RES1(K)=RBIR
      RES2(K)=AR2R
      IF(K.EQ.2) GO TO 155
      K=2
      GO TO 163
C CHECK FOR INTERMEDIATE RIGHT INTERSECTION, EVALUATE IF REQUIRED
182  IF (ISR.NE.10) GO TO 162
      ISR=1
      GO TO 163
162  IF ((RAJR-REJX)/(RAIR-RBIR).GT.0.0) GO TO 163
      AA=(AF2RJ-AR2P)/(RAJR-RAIR)
      EA=AR2P-AA*RAIR
      AB=(AF2RJ-AR2K)/(RBJR-RBIR)
      PB=AR2K-AB*RBIR
      RES1(K)=(EA-PB)/(AA-AB)
      RES2(K)=AA*RES1(K)+EA
      IF(K.EQ.2) GO TO 155
      K=2
C RE-INITIATE
163  AR2FJ=AR2R
      RAJL=RAIL
      RAJR=RAIR
      RBJL=RBIL
      RBJR=RBIR
140  WRITE(6,210)
210  FORMAT(' LOOP 140 THROUGH, NO POINTS FOUND')
      GO TO 155
195  IF (RES1(1).EQ.9000.0) GO TO 191
      IF (RES1(2).EQ.9000.0) GO TO 191
      IF (RES2(1).EQ.9000.0) GO TO 191
      IF (RES2(2).EQ.9000.0) GO TO 191
      GO TO 155
C EVALUATION OF INTERSECTIONS WHEN CURVES ARE ALMOST TANGENT
191  YGC=0.0
      IEPS=2
      CALL PENPTS (I2,N1,X3,Y3,Z3,HT1,YG0,ARRES)
      R1=ABS (ARRES(2)-ARRES(1))/2
      CALL PENPTS (I2,N1,X4,Y4,Z4,HT2,YG0,ARRES)
      R2=ABS (ARRES(2)-ARRES(1))/2
      RES2(1)=((R1**2)-(R2**2)+(ARP2**2))/(2.0*ARP2)
      RES2(2)=RES2(1)
      RES1(1)=SQRT (ABS ((R1**2)-(RES2(1)**2)))
      RES1(2)=-RES1(1)
155  RETURN
      END
      SUBROUTINE PENPTS (IX,IY,X,Y,Z,HT,YG,XR)
      DIMENSION Y (40),ZX(40),Z (40,40),X (40),XR(10)
      IR=1
C SEARCH FOR J OF LOWER Y LINE
      DO 101 I=1,NY
      IF (Y(I).GE.YG) GO TO 102
101  CONTINUE
102  J=I-1
C COARSE SEARCH FOR ZERO PASS
C NEXT 4 LINES ARE EXECUTED IN FIRST SEARCH ONLY
      YC=(YG-Y(J))/(Y(J+1)-Y(J))
      ZX(1)=(Z(1,J+1)-Z(1,J))*YC+Z(1,J)
      IF (ZX(1).EQ.HT) GO TO 107
      I3=2
112  DO 103 I=I3,NX
      ZX(I)=(Z(I,J+1)-Z(I,J))*YC+Z(I,J)
      ZI=(Z(I,J+1)-Z(I-1,J))*(YG-Y(J))/(Y(J+1)-Y(J))+Z(I-1,J)
      IF (ZX(I).EQ.HT) GO TO 103

```

INTC2810
INTC2820
INTC2830
INTC2840
INTC2850
INTC2860
INTC2870
INTC2880
INTC2890
INTC2900
INTC2910
INTC2920
INTC2930
INTC2940
INTC2950
INTC2960
INTC2970
INTC2980
INTC2990
INTC3000
INTC3010
INTC3020
INTC3030
INTC3040
INTC3050
INTC3060
INTC3070
INTC3080
INTC3090
INTC3100
INTC3110
INTC3120
INTC3130
INTC3140
INTC3150
INTC3160
INTC3170
INTC3180
INTC3190
INTC3200
INTC3210
INTC3220
INTC3230
INTC3240
INTC3250
INTC3260
INTC3270
INTC3280
INTC3290
INTC3300
INTC3310
INTC3320
INTC3330
INTC3340
INTC3350
INTC3360
INTC3370
INTC3380
INTC3390
INTC3400
INTC3410
INTC3420
INTC3430
INTC3440
INTC3450
INTC3460
INTC3470
INTC3480
INTC3490
INTC3500

FILE: VUP FORTRAN P1 N P S

```

103 IF ((ZX(I-1)-HT)/(ZX(I)-HT).LT.0.0) GO TO 104
CONTINUE
GO TO 116
C CALCULATION OF PENETRATIONS IN EITHER TRIANGLE
104 XM=X(I-1)+(X(I)-X(I-1))*(YG-Y(J))/(Y(J+1)-Y(J))
IF (ZM.EQ.HT) GO TO 105
IF ((ZX(I)-HT)/(ZM-HT).LT.0.0) GO TO 105
DD=ABS(HT-ZM)+ABS(ZX(I-1)-HT)
XS=X(I-1)+(XM-X(I-1))*ABS(ZX(I-1)-HT)/DD
GO TO 110
105 XS=XM+(X(I)-XM)*ABS(ZM-HT)/(ABS(ZM-HT)+ABS(ZX(I)-HT))
GO TO 110
C LOGICAL PENETRATIONS ACCUMULATION
107 XR(1)=X(1)
I=1
GO TO 113
108 XR(IR)=X(I)
GO TO 111
110 XR(IR)=XS
111 IF (IR.EQ.2) GO TO 114
113 IR=2
IR=I+1
GO TO 114
116 IF (IR.EQ.1) GO TO 117
XR(2)=1000.0
GO TO 114
117 XR(1)=1000.0
XR(2)=1000.0
114 RETURN
END
SUBROUTINE INTPLT(X,Y,Z,XS,YG,AX,NY,ZRES)
C LINEAR INTERPOLATION ON CALIBRATION SURFACE TO EVALUATE
C CP VALUE AT CO-ORDINATES XS,YG. THE RESULT RETURNED IS ZRES
C CP VALUE AT CO-ORDINATES XS,YG. THE RESULT RETURNED IS ZRES
DIMENSION X(40),Y(40),Z(40,40)
C SEARCH FOR I OF LEFT X LINE
DO 1 IC=1,AX
IF (X(IC).GE.XS) GO TO 2
1 CONTINUE
I=IC-1
C SEARCH FOR J OF LOWER Y LINE
DO 3 JC=1,NY
IF (Y(JC).GE.YG) GO TO 4
3 CONTINUE
J=JC-1
4 AL=(Y(J+1)-Y(J))/(X(I+1)-X(I))
BL=Y(J)-AL*X(I)
YCR=(AL*XS)+BL
IF (YG.EQ.YCR) GO TO 7
IF (YG.LT.YCR) GO TO 5
C RESULTING Z IS IN LOWER TRIANGLE
X3=X(I+1)
Y3=Y(J)
Z3=Z(I+1,J)
GO TO 6
C RESULTING Z IS IN UPPER TRIANGLE
5 X3=X(I)
Y3=Y(J+1)
Z3=Z(I,J+1)
GO TO 6
C GENERAL CALCULATION: GOOD FOR BOTH TRIANGLES
6 X1=X(I)
Y1=Y(J)
Z1=Z(I,J)
X2=X(I+1)
Y2=Y(J+1)
Z2=Z(I+1,J+1)
AP=((Z1-Z3)*(Y1-Y2)-(Z1-Z2)*(Y1-Y3))/((X1-X3)*(Y1-Y2)-(X1-X2)
1*(Y1-Y3))
BP=((Z1-Z2)-AP*(X1-X2))/(Y1-Y2)
CP=Z1-AP*X1-BP*Y1
ZRES=AP*XS+BP*YG+CP

```

INTO3510
 INTO3520
 INTO3530
 INTO3540
 INTO3550
 INTO3560
 INTO3570
 INTO3580
 INTO3590
 INTO3600
 INTO3610
 INTO3620
 INTO3630
 INTO3640
 INTO3650
 INTO3660
 INTO3670
 INTO3680
 INTO3690
 INTO3700
 INTO3710
 INTO3720
 INTO3730
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 INTO3780
 INTO3790
 INTO3800
 INTO3810
 INTO3820
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 INTO3840
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 INTO3870
 INTO3880
 INTO3890
 INTO3900
 INTO3910
 INTO3920
 INTO3930
 INTO3940
 INTO3950
 INTO3960
 INTO3970
 INTO3980
 INTO3990
 INTO4000
 INTO4010
 INTO4020
 INTO4030
 INTO4040
 INTO4050
 INTO4060
 INTO4070
 INTO4080
 INTO4090
 INTO4100
 INTO4110
 INTO4120
 INTO4130
 INTO4140
 INTO4150
 INTO4160
 INTO4170
 INTO4180
 INTO4190
 INTO4200

FILE: VDR FORTRAN P1 N P S

```

      GJ TO 100
C RESULTING Z IS ON DIVIDING LINE
7   ZRES=(Z(I+1,J+1)-Z(I,J))*(XG-X(I))/(X(I+1)-X(I))+Z(I,J)
100  RETURN
      END
      SUBROUTINE MAXARY(Z,ZMAX,NX,NY)
C EVALUATION OF MAXIMUM CP OF CALIBRATION SURFACE MATRIX
      DIMENSION Z(40,40)
      DO 1 I=1,NX
      DO 1 J=1,NY
1   IF (Z(I,J).GE.ZMAX) ZMAX=Z(I,J)
      RETURN
      END
      SUBROUTINE MINARY(Z,ZMIN,NX,NY)
C EVALUATION OF MINIMUM CP OF CALIBRATION SURFACE MATRIX
      DIMENSION Z(40,40)
      DO 1 I=1,NX
      DO 1 J=1,NY
1   IF (Z(I,J).LE.ZMIN) ZMIN=Z(I,J)
      RETURN
      END
C END OF VDR

```

```

INTC4210
INTC4220
INTC4230
INTC4240
INTC4250
INTC4260
INTC4270
INTC4280
INTC4290
INTC4300
INTC4310
INTC4320
INTC4330
INTC4340
INTC4350
INTC4360
INTC4370
INTC4380
INTC4390
INTC4400
INTC4410
INTC4420
INTC4430

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APPENDIX 2

LISTING OF SWVDR

C7/C8/75 18.45.15

FILE: SAVOR FORTRAN PL

N

P

S

C START OF SAVOR

DIMENSION ALF(10), PHI(10), XA(40), YA(40),
 ZAX(40,40), XB(40), YB(40), ZB(40,40), XAX(40), YAX(40),
 ZZX(40,40), XBX(40), YBX(40), ZBX(40,40)

119 FORMAT(2I5)

131 FORMAT(F7.1)

130 FORMAT(F5.1)

120 FORMAT(F8.5)

132 FORMAT(F10.5)

135 FORMAT(F15.5)

136 FORMAT(F17.5)

C READ POORE CALIBRATION DATA

READ(2,119) IX, IY

DO 121 I=1, IX

READ(2,130) XA(I)

121 CONTINUE

DO 122 I=1, NY

READ(2,130) YA(I)

122 CONTINUE

DO 123 I=1, NX

DO 123 J=1, NY

READ(2,120) ZA(I,J)

123 CONTINUE

DO 221 I=1, NX

READ(2,130) XB(I)

221 CONTINUE

DO 222 I=1, NY

READ(2,130) YB(I)

222 CONTINUE

DO 223 I=1, NX

DO 223 J=1, NY

READ(2,120) ZB(I,J)

223 CONTINUE

C TRANSFORM CALIBRATION MATRICES

DO 224 I=1, NY

XAX(I)=YA(I)

DO 225 I=1, NX

225 YAX(I)=XA(I)

DO 226 I=1, NY

DO 226 J=1, NX

ZAX(I,J)=ZA(I,J)

226 DO 227 I=1, NY

XBX(I)=YB(I)

227 DO 228 I=1, NX

YBX(I)=XB(I)

228 DO 229 I=1, NY

DO 229 J=1, NX

ZBX(I,J)=ZB(I,J)

229 CONTINUE

C FRCBE SETTINGS

YPA=0.0

YPB=55.

XPA=0.0

XPC=20.

XPD=-20.

C PROGRAM CONSTANTS

YPLD=-30.

YRUP=30.

YRIN=-30.

XRLD=-30.

XRLP=30.

XRIN=-30.

ICOPS=1

NCCOPS=2

NO SIM=2

IIT=1

ISCAN=1

RELXPS=0.5

C EXPERIMENT SIMULATION

153 CONTINUE

401 FORMAT(F15.4)

INT00010

INT00020

INT00030

INT00040

INT00050

INT00060

INT00070

INT00080

INT00090

INT00100

INT00110

INT00120

INT00130

INT00140

INT00150

INT00160

INT00170

INT00180

INT00190

INT00200

INT00210

INT00220

INT00230

INT00240

INT00250

INT00260

INT00270

INT00280

INT00290

INT00300

INT00310

INT00320

INT00330

INT00340

INT00350

INT00360

INT00370

INT00380

INT00390

INT00400

INT00410

INT00420

INT00430

INT00440

INT00450

INT00460

INT00470

INT00480

INT00490

INT00500

INT00510

INT00520

INT00530

INT00540

INT00550

INT00560

INT00570

INT00580

INT00590

INT00600

INT00610

INT00620

INT00630

INT00640

INT00650

INT00660

INT00670

INT00680

INT00690

INT00700

FILE: SWVDR FCRTRAN P1

N

P

S

```

READ(5,401) PT
WRITE(6,401) PT
IF(NCSIM.EQ.2) GO TO 500
READ(5,401) PS
WRITE(6,401) PS
READ(5,401) ALFA
WRITE(6,401) ALFA
READ(5,401) PHII
WRITE(6,401) PHII
CALL INTPLT(XA,YA,ZA,ALFA,PHII,NX,NY,CPA)
ALFC=ALFA-APC
CALL INTPLT(XA,YA,ZA,ALFC,PHII,NX,NY,CPC)
ALFL=ALFA-APC
CALL INTPLT(XA,YA,ZA,ALFL,PHII,NX,NY,CPD)
PHIB=PHII-YPB
CALL INTPLT(XB,YB,ZB,ALFA,PHIB,NX,NY,CPB)
PDYN=PT-PS
PPA=CPA*PDYN+PS
PFB=CFC*PDYN+PS
PPC=CPC*PDYN+PS
PFD=CPD*PDYN+PS
C READ MEASUREMENTS DATA
IF(NCSI4.EQ.1) GO TO 501
500 READ(5,135) PPA
WRITE(6,135) PPA
READ(5,135) PPB
WRITE(6,135) PPB
READ(5,135) PPC
WRITE(6,135) PPC
READ(5,135) PPD
WRITE(6,135) PPD
501 READ(5,135) PSIN
WRITE(6,135) PSIN
IF(ISCAN.EQ.1) GO TO 181
180 IF(ISCAN.GT.1000) GO TO 305
II=I
ICCP5=1
ISCAN=ISCAN+1
PSIN=PSIN+5.0
WRITE(6,135) PSIN
181 CONTINUE
PS=PSIN
FSC=PSIN
PST=PS
C CALCULATES PRESSURE COEFFICIENTS
300 CONTINUE
PDYN=PT-PS
CPA=(PPA-PS)/PDYN
CFE=(PFE-PS)/PDYN
CPC=(PPC-PS)/PDYN
CPD=(PPE-PS)/PDYN
C CORRECTS PS ASSUMPTION TO ENSURE CF ARE IN CALIBRATION RANGE
IF(NDCPS.EQ.2) GO TO 301
ZAMAX=-10000.
CALL MAXARY(ZA,ZAMAX,NX,NY)
IF(CPA.GT.ZAMAX) PSC=1.01*PS
IF(CFC.GT.ZAMAX) PSC=1.01*PS
IF(CPD.GT.ZAMAX) PSC=1.01*PS
ZBMAX=-10000.
CALL MAXARY(ZB,ZBMAX,NX,NY)
IF(CPB.GT.ZBMAX) PSC=1.01*PS
ZAMIN=10000.
CALL MINARY(ZA,ZAMIN,NX,NY)
IF(CPA.LT.ZAMIN) PSC=0.99*PS
IF(CFC.LT.ZAMIN) PSC=0.99*PS
IF(CPD.LT.ZAMIN) PSC=0.99*PS
ZBMIN=10000.
CALL MINARY(ZB,ZBMIN,NX,NY)
IF(CPB.LT.ZBMIN) PSC=0.99*PS
IF(PSC.EQ.PST) GO TO 301

```

INTCC710
INTCC720
INTCC730
INTCC740
INTCC750
INTCC760
INTCC770
INTCC780
INTCC790
INTCC800
INTCC810
INTCC820
INTCC830
INTCC840
INTCC850
INTCC860
INTCC870
INTCC880
INTCC890
INTCC900
INTCC910
INTCC920
INTCC930
INTCC940
INTCC950
INTCC960
INTCC970
INTCC980
INTCC990
INTC1000
INTC1010
INTC1020
INTC1030
INTC1040
INTC1050
INTC1060
INTC1070
INTC1080
INTC1090
INTC1100
INTC1110
INTC1120
INTC1130
INTC1140
INTC1150
INTC1160
INTC1170
INTC1180
INTC1190
INTC1200
INTC1210
INTC1220
INTC1230
INTC1240
INTC1250
INTC1260
INTC1270
INTC1280
INTC1290
INTC1300
INTC1310
INTC1320
INTC1330
INTC1340
INTC1350
INTC1360
INTC1370
INTC1380
INTC1390
INTC1400

```

      ICOPS=ICOPS+1
      IF (ICOPS.GT.10) GO TO 180
      PS=PSC
      PST=PSC
      GO TO 300
301  CONTINUE
      C CALCULATES TWO ALF & PHI ANGLES FOR 'I' & 'II'
      CALL INTSCS (YPA,YPB,YRL,YRUP,YRIN,
      1CPA,CPS,ALF,PHI,XA,YA,ZA,
      2XB,YB,ZB,XAX,YAX,ZAX,XBX,YBX,ZBX,NX,NY)
      ALF1=ALF(1)
      ALF2=ALF(2)
      PHI1=PHI(1)
      PHI2=PHI(2)
      C CALCULATES TWO ALF & PHI ANGLES FOR 'I' & 'III'
      CALL INTSCS (XPA,XPC,XRL,XRUP,XRIN,
      1CPA,CPC,PHI,ALF,XAX,YAX,ZAX,
      2XAX,YAX,ZAX,XA,YA,ZA,XA,YA,ZA,NY,NX)
      ALF3=ALF(1)
      ALF4=ALF(2)
      PHI3=PHI(1)
      PHI4=PHI(2)
      C SELECTS THE PROPER ALF & PHI ANGLES OUT OF THE FOUR VALUES
      FALF=((ALF1+ALF2+ALF3+ALF4)-AMAX1(ALF1,ALF2,ALF3,
      1ALF4)-AMIN1(ALF1,ALF2,ALF3,ALF4))/2
      FPHI=((PHI1+PHI2+PHI3+PHI4)-AMAX1(PHI1,PHI2,PHI3,PHI4)
      1-AMIN1(PHI1,PHI2,PHI3,PHI4))/2
      C CALCULATES NEW PS FROM DATA OF POSITION D AND CORRECTS PT
      ALFON=FALF-XPD
      CALL INTCT(XA,YA,ZA,ALFON,FPHI,NX,NY,CPC)
      ALFON=FALF-XPC
      CALL INTCT(XA,YA,ZA,ALFON,FPHI,NX,NY,CPC)
      PSN=(PPC*CPU-PPD*CPC)/(CPU-CPC)
907  WRITE(5,511) IIT,FALF,FPHI,PSN
911  FORMAT(' ITERATION VALUES ',15,10X,2F6.2,F10.2)
      C CONVERGENCE TESTS
      EPSPS=ABS((PSN-PS)/PS)
      EPSPSG=.00000000009*(PT**2.0)-.00000008*PT
      IF (1/PSN.EQ.2) EPSPSG=.0000000009*(PT**2.0)-.0000008*PT
      IF (1/EPSP2.EQ.2) EPSPSG=.0000000009*(PT**2.0)-.0000008*PT
      IF (EPSPS.GT.EPSPSG) GO TO 310
      GO TO 300
310  CONTINUE
      IIT=IIT+1
      IF (IIT.GT.10) GO TO 180
      PS=PS+RELXPS*(PSN-PS)
      PSC=PS
      PST=PS
      GO TO 300
303  WRITE(5,171) FALF
171  FORMAT('01',' VELOCITY YAW IS' ,F15.2)
      WRITE(5,172) FPHI
172  FORMAT(' VELOCITY PITCH IS' ,F15.2)
      WRITE(5,173) PSN
173  FORMAT(' STATIC PRESSURE IS' ,F15.3)
      WRITE(5,174) PT
174  FORMAT(' TOTAL PRESSURE IS' ,F15.3)
      AM=SGRT(((PT/PSN)**0.285714-1.0)*5.0)
      WRITE(5,175) AM
175  FORMAT(' MACH NUMBER IS' ,F15.5)
      GO TO 193
305  WRITE(5,307)
307  FORMAT(' SCANNED 1000 TIMES')
      GO TO 193
      END
      SUBROUTINE INTSCS (ARP1,ARP2,ARLO,ARUP,ARIN,
      1HT1,HT2,RES1,RES2,X1,Y1,Z1,
      2X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,N1,N2)
      DIMENSION RES1(10),RES2(10),ARRES(10),X1(40),Y1(40),
      1Z1(40,40),X2(40),Y2(40),Z2(40,40),X3(40),Y3(40),

```

INTC1410
INTC1420
INTC1430
INTC1440
INTC1450
INTC1460
INTC1470
INTC1480
INTC1490
INTC1500
INTC1510
INTC1520
INTC1530
INTC1540
INTC1550
INTC1560
INTC1570
INTC1580
INTC1590
INTC1600
INTC1610
INTC1620
INTC1630
INTC1640
INTC1650
INTC1660
INTC1670
INTC1680
INTC1690
INTC1700
INTC1710
INTC1720
INTC1730
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INTC1780
INTC1790
INTC1800
INTC1810
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INTC1870
INTC1880
INTC1890
INTC1900
INTC1910
INTC1920
INTC1930
INTC1940
INTC1950
INTC1960
INTC1970
INTC1980
INTC1990
INTC2000
INTC2010
INTC2020
INTC2030
INTC2040
INTC2050
INTC2060
INTC2070
INTC2080
INTC2090
INTC2100

```

      ZJ(40,40),X4(40),Y4(40),Z+(40,40)
      RES1(1)=9000.
      RES1(2)=9000.
      RES2(1)=9000.
      RES2(2)=9000.
      ISL=1
      ISR=1
      DAR=1.
      ARZR=AR*IN
      GO TO 152
150  ARZR=ARZR+DAR
      ARZRJ=ARZR
152  ARM1=ARZR-ARP1
      ARM2=ARZR-ARP2
C CHECK FOR LOWER CALIBRATION RANGE
      IF (ARM1.LT.ARLD) GO TO 150
      IF (ARM2.LT.ARLD) GO TO 150
      K=1
C CALCULATES INITIAL PENETRATION POINTS
      CALL PENPTS(N1,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
      RAJL=ARRES(1)
      RAJR=ARRES(2)
      CALL PENPTS(N1,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
      RBJL=ARRES(1)
      RBJR=ARRES(2)
C CALCULATES SUCCESSIVE PENETRATION POINTS
      DO 140 I=1,10000
      ARZR=ARZR+DAR
      ARM1=ARZR-ARP1
      ARM2=ARZR-ARP2
C CHECK FOR UPPER CALIBRATION RANGE
      IF (ARM1.GT.ARUP) GO TO 195
      IF (ARM2.GT.ARUP) GO TO 195
      CALL PENPTS(N1,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
      RAIL=ARRES(1)
      RAIR=ARRES(2)
      CALL PENPTS(N1,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
      RBIL=ARRES(1)
      RBIR=ARRES(2)
      IF (RAJL.EQ.1000.) ISL=10
      IF (REJL.EQ.1000.) ISL=10
      IF (RAJR.EQ.1000.) ISR=10
      IF (REJR.EQ.1000.) ISR=10
      IF (RAIL.EQ.1000.) ISL=10
      IF (REIL.EQ.1000.) ISL=10
      IF (RAIR.EQ.1000.) ISR=10
      IF (REIR.EQ.1000.) ISR=10
C CHECK FOR DIRECT HIT TO LEFT INTERSECTION,EVALUATE IF REQUIRED
      IF (ISL.NE.10) GO TO 164
      ISL=1
      GO TO 183
164  IF (RAIL.NE.RBIL) GO TO 180
      RES1(K)=RBIL
      RES2(K)=ARZR
      IF (K.EQ.2) GO TO 155
      K=2
      GO TO 183
C CHECK FOR INTERMEDIATE LEFT INTERSECTION,EVALUATE IF REQUIRED
180  IF (ISL.NE.10) GO TO 160
      ISL=1
      GO TO 183
160  IF ((RAJL-RBIL)/(RAIL-RBIL).GT.0.0) GO TO 183
      AA=(ARZRJ-ARZR)/(RAJL-RAIL)
      BA=ARZR-AA*RAIL
      AB=(ARZRJ-ARZR)/(REJL-RBIL)
      BB=ARZR-AB*RBIL
      RES1(K)=(BA-RA)/(AA-AB)
      RES2(K)=AA*RES1(K)+BA
      IF (K.EQ.2) GO TO 155
      K=2

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INTC2110
INTC2120
INTC2130
INTC2140
INTC2150
INTC2160
INTC2170
INTC2180
INTC2190
INTC2200
INTC2210
INTC2220
INTC2230
INTC2240
INTC2250
INTC2260
INTC2270
INTC2280
INTC2290
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INTC2500
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INTC2770
INTC2780
INTC2790
INTC2800

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FILE: SWVR      FORTRAN P1      N      P      S

C CHECK FOR DIRECT HIT IN RIGHT INTERSECTION, EVALUATE IF REQUIRED
185 IF (ISR.NE.10) GO TO 161
    ISR=1
    GO TO 163
161 IF (RAJR.NE.RBIR) GO TO 182
    RES1(N)=RAJR
    RES2(K)=RBIR
    IF (K.EQ.2) GO TO 155
    K=2
    GO TO 163
C CHECK FOR INTERMEDIATE RIGHT INTERSECTION, EVALUATE IF REQUIRED
182 IF (ISR.NE.10) GO TO 162
    ISR=1
    GO TO 163
162 IF ((RAJR-RBJR)/(PAIR-RBIR).GT.0.0) GO TO 163
    AA=(AP2RJ-AR2R)/(RAJR-RAIR)
    EA=AR2R-AA*RAIR
    AB=(AP2RJ-AR2R)/(RBJR-RBIR)
    EB=AR2R-AB*RBIR
    RES1(K)=(EA-EB)/(AA-AB)
    RES2(K)=AA*RES1(K)+EA
    IF (K.EQ.2) GO TO 155
    K=2
C RE-INITIATE
163 AR2RJ=AR2R
    RAJR=PAIR
    PAJR=PAIR
    RBJR=RBIR
    RBJR=PAIR
140 CONTINUE
    WRITE(6,210)
210 FORMAT(' LOOP 140 THROUGH, NO POINTS FOUND')
    GO TO 155
195 IF (RES1(1).EQ.9999.0) GO TO 191
    IF (RES1(2).EQ.9999.0) GO TO 191
    IF (RES2(1).EQ.9999.0) GO TO 191
    IF (RES2(2).EQ.9999.0) GO TO 191
    GO TO 155
C EVALUATION OF INTERSECTIONS WHEN CURVES ARE ALMOST TANGENT
191 YG=0.0
    CALL PENPTS(N2,N1,X3,Y3,Z3,HT1,YC,ARRES)
    R1=ABS(ARRES(2)-ARRES(1))/2
    CALL PENPTS(N2,N1,X4,Y4,Z4,HT2,YG,ARRES)
    R2=ABS(ARRES(2)-ARRES(1))/2
    RES2(1)=((R1**2)-(R2**2)+(ARP2**2))/(2.0*ARP2)
    RES2(2)=RES2(1)
    RES1(1)=SIGN(ABS((R1**2)-(RES2(1)**2)))
    RES1(2)=-RES1(1)
155 RETURN
    END
    SUBROUTINE PENPTS(NX,NY,X,Y,Z,HT,YG,XR)
    DIMENSION Y(40),Z(40),Z(40,40),X(40),XR(10)
    IR=1
C SEARCH FOR J OF LOWER Y LINE
    DO 101 I=1,NY
    101 IF (Y(I).GE.YG) GO TO 102
    CONTINUE
102 J=I-1
C CHOOSE SCAN FOR ZERO PASS
C NEXT + LINES ARE EXECUTED IN FIRST SEARCH ONLY
    YC=(YG-Y(J))/(Y(J+1)-Y(J))
    ZX(1)=(Z(1,J+1)-Z(1,J))*YC+Z(1,J)
    IF (ZX(1).EQ.HT) GO TO 107
    IR=2
112 DO 103 I=1B,IX
    ZX(I)=(Z(1,J+1)-Z(1,J))*YC+Z(1,J)
    ZI=(Z(1,J+1)-Z(1-1,J))*(Y(J+1)-Y(J))/(Y(J+1)-Y(J))+Z(1-1,J)
    IF (ZX(I).EQ.HT) GO TO 108
    IF ((ZX(I)-HT)/(ZX(1)-HT).LT.0.0) GO TO 104
103 CONTINUE

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INTC2810
INTC2820
INTC2830
INTC2840
INTC2850
INTC2860
INTC2870
INTC2880
INTC2890
INTC2900
INTC2910
INTC2920
INTC2930
INTC2940
INTC2950
INTC2960
INTC2970
INTC2980
INTC2990
INTC3000
INTC3010
INTC3020
INTC3030
INTC3040
INTC3050
INTC3060
INTC3070
INTC3080
INTC3090
INTC3100
INTC3110
INTC3120
INTC3130
INTC3140
INTC3150
INTC3160
INTC3170
INTC3180
INTC3190
INTC3200
INTC3210
INTC3220
INTC3230
INTC3240
INTC3250
INTC3260
INTC3270
INTC3280
INTC3290
INTC3300
INTC3310
INTC3320
INTC3330
INTC3340
INTC3350
INTC3360
INTC3370
INTC3380
INTC3390
INTC3400
INTC3410
INTC3420
INTC3430
INTC3440
INTC3450
INTC3460
INTC3470
INTC3480
INTC3490
INTC3500

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      GO TO 116
C CALCULATION OF PENETRATIONS IN EITHER TRIANGLE
104 XM=X(I-1)+(X(I)-X(I-1))*(YG-Y(J))/(Y(J+1)-Y(J))
      IF(ZM.EQ.HT) GO TO 105
      IF((ZX(I)-HT)/(ZM-HT).LT.0.0) GO TO 105
      DU=ABS(HT-ZM)+ABS(ZX(I-1)-HT)
      XS=(I-1)+(XM-X(I-1))*ABS(ZX(I-1)-HT)/DU
      GO TO 110
105 XS=X+(X(I)-XM)*ABS(ZM-HT)/(ABS(ZM-HT)+ABS(ZX(I)-HT))
      GO TO 110
C LOCAL PENETRATIONS ACCUMULATION
107 XR(1)=X(I)
      I=1
      GO TO 113
108 XR(IR)=X(I)
      GO TO 111
110 XR(IR)=XS
111 IF(IR.EQ.2) GO TO 114
113 IR=2
      IB=I+1
      GO TO 112
116 IF(IF.EQ.1) GO TO 117
      XR(2)=1000.0
      GO TO 114
117 XR(1)=1000.0
      XR(2)=1000.0
114 RETURN
      END
      SUBROUTINE INTPLT(X,Y,Z,XS,YG,NX,NY,ZRES)
C LINEAR INTERPOLATION ON CALIBRATION SURFACE TO EVALUATE
C CP VALUE AT CO-ORDINATES XS,YG. THE RESULT RETURNED IS ZRES
      DIMENSION X(40),Y(40),Z(40,40)
C SEARCH FOR I OF LEFT X LINE
      DO 1 IC=1,NX
      IF(X(IC).GE.XG) GO TO 2
1      CONTINUE
2      I=IC-1
C SEARCH FOR J OF LOWER Y LINE
      DO 3 JC=1,NY
      IF(Y(JC).GE.YG) GO TO 4
3      CONTINUE
4      J=JC-1
      AL=(Y(J+1)-Y(J))/(X(I+1)-X(I))
      BL=Y(J)-AL*X(I)
      YCR=(AL*XS)+BL
      IF(YG.EQ.YCR) GO TO 7
      IF(YG.GT.YCR) GO TO 5
C RESULTING Z IS IN LOWER TRIANGLE
      X3=X(I+1)
      Y3=Y(J)
      Z3=Z(I+1,J)
      GO TO 6
C RESULTING Z IS IN UPPER TRIANGLE
5      X3=X(I)
      Y3=Y(J+1)
      Z3=Z(I,J+1)
C GENERAL CALCULATION: GOOD FOR BOTH TRIANGLES
6      X1=X(I)
      Y1=Y(J)
      Z1=Z(I,J)
      X2=X(I+1)
      Y2=Y(J+1)
      Z2=Z(I+1,J+1)
      AP=((Z1-Z3)*(Y1-Y2)-(Z1-Z2)*(Y1-Y3))/((X1-X3)*(Y1-Y2)-(X1-X2)
1*(Y1-Y3))
      BP=((Z1-Z2)-AP*(X1-X2))/(Y1-Y2)
      CP=Z1-AP*X1-BP*Y1
      ZRES=AP*XS+BP*YG+CP
      GO TO 100
C RESULTING Z IS ON DIVIDING LINE

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INT03510
INT03520
INT03530
INT03540
INT03550
INT03560
INT03570
INT03580
INT03590
INT03600
INT03610
INT03620
INT03630
INT03640
INT03650
INT03660
INT03670
INT03680
INT03690
INT03700
INT03710
INT03720
INT03730
INT03740
INT03750
INT03760
INT03770
INT03780
INT03790
INT03800
INT03810
INT03820
INT03830
INT03840
INT03850
INT03860
INT03870
INT03880
INT03890
INT03900
INT03910
INT03920
INT03930
INT03940
INT03950
INT03960
INT03970
INT03980
INT03990
INT04000
INT04010
INT04020
INT04030
INT04040
INT04050
INT04060
INT04070
INT04080
INT04090
INT04100
INT04110
INT04120
INT04130
INT04140
INT04150
INT04160
INT04170
INT04180
INT04190
INT04200

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INTC4210
INTC4220
INTC4230
INTC4240
INTC4250
INTC4260
INTC4270
INTC4280
INTC4290
INTC4300
INTC4310
INTC4320
INTC4330
INTC4340
INTC4350
INTC4360
INTC4370
INTC4380
INTC4390
INTC4400
INTC4410

APPENDIX 3

LISTING OF WVDR

07/08/75 18.45.53

FILE: WVER FORTRAN P1

N P

S

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C START OF WVER
      GIVEASIN ALF(10),PHI(10),XA(40),YA(40),
      1ZA(40,40),XB(40),YB(40),ZP(40,40),XAX(40),YAX(40),
      2ZAX(40,40),XBX(40),YBX(40),ZBX(40,40)
119   FORMAT(215)
131   FORMAT(F7.1)
130   FORMAT(F5.1)
120   FORMAT(F6.5)
132   FORMAT(F10.5)
135   FORMAT(F15.5)
136   FORMAT(F17.5)
C READ POLYMER CALIBRATION DATA
      READ(2,119) XA,YA
      DO 121 I=1,NX
      READ(2,130) XA(I)
121   CONTINUE
      DO 122 I=1,NY
      READ(2,130) YA(I)
122   CONTINUE
      DO 123 I=1,NX
      DO 123 J=1,NY
      READ(2,120) ZA(I,J)
123   CONTINUE
      DO 221 I=1,NX
      READ(2,130) XB(I)
221   CONTINUE
      DO 222 I=1,NY
      READ(2,130) YB(I)
222   CONTINUE
      DO 223 I=1,NX
      DO 223 J=1,NY
      READ(2,120) ZB(I,J)
223   CONTINUE
C TRANSFORM CALIBRATION MATRICES
      DO 224 I=1,NY
224   XAX(I)=YA(I)
      DO 225 I=1,NX
225   YAX(I)=XA(I)
      DO 226 I=1,NY
      DO 226 J=1,NX
226   ZAX(I,J)=ZA(J,I)
      DO 227 I=1,NY
227   XBX(I)=YB(I)
      DO 228 I=1,NX
228   YBX(I)=XB(I)
      DO 229 I=1,NY
      DO 229 J=1,NX
229   ZBX(I,J)=ZB(J,I)
C FREQUENCY SETTINGS
      YPA=0.0
      YPB=55.
      XPA=0.0
      XPC=20.
      XPD=-20.
C PROGRAM CONSTANTS
      YRLC=-30.
      YRLP=30.
      YRLN=-30.
      XRLC=-30.
      XRLP=30.
      XRLN=-30.
      ICCPS=1
      NUCCPS=2
      NOSIM=1
      IIT=1
      ISCAN=1
      RELXFS=0.5
C EXPERIMENT SIMULATION
195   CONTINUE
401   FORMAT(F15.4)

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INT00010
INT00020
INT00030
INT00040
INT00050
INT00060
INT00070
INT00080
INT00090
INT00100
INT00110
INT00120
INT00130
INT00140
INT00150
INT00160
INT00170
INT00180
INT00190
INT00200
INT00210
INT00220
INT00230
INT00240
INT00250
INT00260
INT00270
INT00280
INT00290
INT00300
INT00310
INT00320
INT00330
INT00340
INT00350
INT00360
INT00370
INT00380
INT00390
INT00400
INT00410
INT00420
INT00430
INT00440
INT00450
INT00460
INT00470
INT00480
INT00490
INT00500
INT00510
INT00520
INT00530
INT00540
INT00550
INT00560
INT00570
INT00580
INT00590
INT00600
INT00610
INT00620
INT00630
INT00640
INT00650
INT00660
INT00670
INT00680
INT00690
INT00700

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      READ(5,401) PT
      WRITE(6,401) PT
      IF (NCSIM.EQ.2) GO TO 500
      READ(5,401) PS
      WRITE(6,401) PS
      READ(5,401) ALFA
      WRITE(6,401) ALFA
      READ(5,401) PHII
      WRITE(6,401) PHII
      CALL INTPLT(XA,YA,ZA,ALFA,PHII,IX,NY,CPA)
      ALFC=ALFA-XPC
      CALL INTPLT(XA,YA,ZA,ALFC,PHII,IX,NY,CPC)
      ALFD=ALFA-XPC
      CALL INTPLT(XA,YA,ZA,ALFD,PHII,IX,NY,CPC)
      PHIR=PHII-YP
      CALL INTPLT(XA,YA,ZA,ALFA,PHIR,IX,NY,CPR)
      WRITE(6,402) CPA,CPC,CPC,CPC
      FORMAT(' TRUE CPS ',4F10.5)
402  PDYN=PT-PS
      PPA=CPA*PDYN+PS
      PPR=CPC*PDYN+PS
      PPC=CPC*PDYN+PS
      PPD=CPC*PDYN+PS
      WRITE(6,403) PPA,PPR,PPC,PPD
403  FORMAT(' SIMUL PHS ',4F10.2)
C READ MEASUREMENTS DATA
      IF (NCSIM.EQ.1) GO TO 501
500  READ(5,135) PPA
      WRITE(6,135) PPA
      READ(5,135) PPR
      WRITE(6,135) PPR
      READ(5,135) PPC
      WRITE(6,135) PPC
      READ(5,135) PPD
      WRITE(6,135) PPD
501  READ(5,135) PSIN
      WRITE(6,135) PSIN
      IF (ISCAN.EQ.1) GO TO 181
180  IF (ISCAN.GT.1000) GO TO 305
      IIT=1
      ICPS=1
      ISCAN=ISCAN+1
      PSIN=PSIN+5.0
      WRITE(6,135) PSIN
181  CONTINUE
      FS=PSIN
      PSC=PS
      PST=PS
C CALCULATES PRESSURE COEFFICIENTS
300  CONTINUE
      WRITE(6,940) IIT
940  FORMAT(' I ',11X,' IIT-ATION NO. ',15)
      PDYN=PT-PS
      CPA=(PPA-PS)/PDYN
      CPB=(PPR-PS)/PDYN
      CPC=(PPC-PS)/PDYN
      CPD=(PPD-PS)/PDYN
908  WRITE(6,912) CPA,CPB,CPC,CPD
912  FORMAT(' CLC CPS ',4F10.5)
C CORRECTS PS ASSUMPTION TO ENSURE CP ARE IN CALIBRATION RANGE
      IF (NCCPS.EQ.2) GO TO 501
      ZAMAX=-1000.0
      CALL MAXXY(2,ZAMAX,IX,NY)
      IF (CPA.GT.ZAMAX) PSC=1.01*PS
      IF (CPB.GT.ZAMAX) PSC=1.01*PS
      IF (CPD.GT.ZAMAX) PSC=1.01*PS
      ZAMAX=-1000.0
      CALL MAXXY(2,ZAMAX,IX,NY)
      IF (CPC.GT.ZAMAX) PSC=1.01*PS
      ZAMIN=1000.0

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INT00710
INT00720
INT00730
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INT00990
INT01000
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INT01120
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INT01140
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INT01160
INT01170
INT01180
INT01190
INT01200
INT01210
INT01220
INT01230
INT01240
INT01250
INT01260
INT01270
INT01280
INT01290
INT01300
INT01310
INT01320
INT01330
INT01340
INT01350
INT01360
INT01370
INT01380
INT01390
INT01400

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```

      CALL MINARY(ZA,ZAMIN,NX,NY)
      IF(CPA.LT.ZAMIN) PSC=C.99*PS
      IF(CPC.LT.ZAMIN) PSC=C.99*PS
      IF(CPD.LT.ZAMIN) PSC=C.99*PS
      ZBMIN=10000.
      CALL MINARY(ZB,ZBMIN,NX,NY)
      IF(CPB.LT.ZBMIN) PSC=C.99*PS
      IF(PSC.EQ.PST) GO TO 301
      ICCPS=ICCPST+1
963 WRITE(6,964) ICCPS
964 FORMAT(' ICCPS IS',15)
      IF(ICCPS.GT.10) GO TO 180
      PS=PSC
      PST=PSC
920 WRITE(6,921) PSC
921 FORMAT(' PSC IS',F20.5)
      GO TO 300
301 CONTINUE
C CALCULATES TWO ALF & PHI ANGLES FOR 'I' & 'III'
      CALL INTSCS(YPA,YPB,YRLO,YRUP,YRIN,
      1CPA,CPC,ALF,PHI,XA,YA,ZA,
      2XB,YB,ZB,XAX,YAX,ZAX,XEX,YEX,ZBX,NX,NY)
      ALF1=ALF(1)
      ALF2=ALF(2)
      PHI1=PHI(1)
      PHI2=PHI(2)
C CALCULATES TWO ALF & PHI ANGLES FOR 'I' & 'III'
      CALL INTSCS(XPA,XPC,XRLO,XRUP,XRIN,
      1CPA,CPC,PHI,ALF,XAX,YAX,ZAX,
      2XAX,YAX,ZAX,XA,YA,ZA,XA,YA,ZA,NX,NY)
      ALF3=ALF(1)
      ALF4=ALF(2)
      PHI3=PHI(1)
      PHI4=PHI(2)
C SELECTS THE PROPER ALF & PHI ANGLES OUT OF THE FOUR VALUES
      FALF=((ALF1+ALF2+ALF3+ALF4)-AMAX1(ALF1,ALF2,ALF3,
      1ALF4)-AMIN1(ALF1,ALF2,ALF3,ALF4))/2
      FPHI=((PHI1+PHI2+PHI3+PHI4)-AMAX1(PHI1,PHI2,PHI3,PHI4)
      1-AMIN1(PHI1,PHI2,PHI3,PHI4))/2
900 WRITE(6,901) FALF,FPHI
901 FORMAT(' SELECTED',2F10.2)
C CALCULATES NEW PS FROM DATA OF POSITION D AND CORRECTS PT
      ALFON=FALF-XPD
      CALL INTPLT(XA,YA,ZA,ALFON,FPHI,NX,NY,CPD)
      ALFCN=FALF-XPC
      CALL INTPLT(XA,YA,ZA,ALFCN,FPHI,NX,NY,CPC)
905 WRITE(6,910) CPC,CPD
910 FORMAT(' NEW CPC & CPD CALLED',2F15.5)
      PSN=(PPC*CPD-PPD*CPC)/(CPD-CPC)
907 WRITE(6,911) FALF,FPHI,PSN,PT
911 FORMAT(' ITERATION VALUES',2F6.2,2F10.2)
C CONVERGENCE TESTS
950 DELPS=PSN-PS
951 WRITE(6,952) PS,FPHI,DELPS
952 FORMAT(' EPSPS VALUES',3F15.5)
      EPSPS=ABS((PSN-PS)/PS)
960 WRITE(6,961) EPSPS
961 FORMAT(' EPSPS IS',F25.15)
      EPSPSG=.00000000099*(PT**2.0)-.000000098*PT
      IF(IEPS1.EQ.2) EPSPSG=.00000000099*(PT**2.0)-.00000008*PT
      IF(IEPS2.EQ.2) EPSPSG=.00000000099*(PT**2.0)-.00000008*PT
      IF(EPSPS.GT.EPSPSG) GO TO 310
      GO TO 302
310 CONTINUE
      IIT=IIT+1
      IF(IIT.GT.10) GO TO 305
      PS=PS+RELXPS*(PSN-PS)
      PSC=PS
      PST=PS
924 WRITE(6,925) PS

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INT01410
INT01420
INT01430
INT01440
INT01450
INT01460
INT01470
INT01480
INT01490
INT01500
INT01510
INT01520
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INT01540
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INT01570
INT01580
INT01590
INT01600
INT01610
INT01620
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INT01690
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INT01950
INT01960
INT01970
INT01980
INT01990
INT02000
INT02010
INT02020
INT02030
INT02040
INT02050
INT02060
INT02070
INT02080
INT02090
INT02100

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FILE: WDR FORTRAN P1 N P S

```

925 FORMAT(' CURR PS IS ',F15.5)
GO TO 300
303 WRITE(6,171) FALF,FPF1,PSN,PT
171 FORMAT('JF15.2,F15.3')
GO TO 193
305 WRITE(6,307)
307 FORMAT(' SCANNED 100 TIMES')
GO TO 193
END
SUBROUTINE INTSCS(ARP1,ARP2,ARL0,ARUP,ARIN,
1HT1,HT2,RES1,RES2,X1,Y1,Z1,
2X2,Y2,Z2,X3,Y3,Z3,X4,Y4,Z4,N1,N2)
DIMENSION RES1(10),ARRES(10),A1(40),Y1(40),
1Z1(40,40),X2(40),Y2(40),Z2(40,40),X3(40),Y3(40),
2Z3(40,40),X4(40),Y4(40),Z4(40,40)
RES1(1)=9000.
RES1(2)=9000.
RES2(1)=9000.
RES2(2)=9000.
ISL=1
ISR=1
DAR=1.
ARZR=ARIN
GO TO 152
150 ARZR=ARZR+DAR
ARZRJ=ARZR
152 ARM1=ARZR-ARP1
ARM2=ARZR-ARP2
C CHECK FOR LOWER CALIBRATION RANGE
IF (ARM1.LT.ARL0) GO TO 150
IF (ARM2.LT.ARL0) GO TO 150
K=1
C CALCULATES INITIAL PENETRATION POINTS
CALL PENPTS(11,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJR=ARRES(2)
CALL PENPTS(11,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBJL=ARRES(1)
RBJR=ARRES(2)
C CALCULATES SUCCESSIVE PENETRATION POINTS
DO 140 I=1,10000
ARZR=ARZR+DAR
ARM1=ARZR-ARP1
ARM2=ARZR-ARP2
C CHECK FOR UPPER CALIBRATION RANGE
IF (ARM1.GT.ARUP) GO TO 195
IF (ARM2.GT.ARUP) GO TO 195
CALL PENPTS(11,N2,X1,Y1,Z1,HT1,ARM1,ARRES)
RAJL=ARRES(1)
RAJR=ARRES(2)
CALL PENPTS(11,N2,X2,Y2,Z2,HT2,ARM2,ARRES)
RBJL=ARRES(1)
RBJR=ARRES(2)
IF (RAJL.EQ.1000.) ISL=10
IF (RAJR.EQ.1000.) ISL=10
IF (RBJR.EQ.1000.) ISR=10
IF (RAJR.EQ.1000.) ISR=10
IF (RAJL.EQ.1000.) ISL=10
IF (RBIL.EQ.1000.) ISL=10
IF (RBIR.EQ.1000.) ISR=10
IF (RAJR.EQ.1000.) ISR=10
C CHECK FOR DIRECT HIT ON LEFT INTERSECTION, EVALUATE IF REQUIRED
IF (ISL.NE.10) GO TO 164
ISL=1
GO TO 183
164 IF (RAJL.NE.RBIL) GO TO 180
RES1(K)=RBIL
RES2(K)=ARZR
IF (K.EQ.2) GO TO 155
K=2

```

INTO2110
 INTO2120
 INTO2130
 INTO2140
 INTO2150
 INTO2160
 INTO2170
 INTO2180
 INTO2190
 INTO2200
 INTO2210
 INTO2220
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 INTO2240
 INTO2250
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 INTO2770
 INTO2780
 INTO2790
 INTO2800

```

      GO TO 185
C CHECK FOR INTERMEDIATE LEFT INTERSECTION,EVALUATE IF REQUIRED
180 IF (ISL.NE.10) GO TO 160
      ISL=1
      GO TO 183
160 IF ((FAJL-RBJL)/(FAIL-RBIL).GT.0.0) GO TO 183
      AA=(AF2RJ-AR2K)/(RAJL-RAIL)
      EA=AR2K-AA*RAIL
      AB=(AR2KJ-AR2K)/(FBJL-FBIL)
      BB=AR2K-AB*FBIL
      RES1(K)=(EB-EA)/(AA-AB)
      RES2(K)=AA*RES1(K)+EA
      IF (K.EQ.2) GO TO 155
      K=2
C CHECK FOR DIRECT HIT JJ RIGHT INTERSECTION,EVALUATE IF REQUIRED
183 IF (ISR.NE.10) GO TO 161
      ISR=1
      GO TO 163
161 IF (RAIK.NE.RBIR) GO TO 182
      RES1(K)=RBIR
      RES2(K)=AR2K
      IF (K.EQ.2) GO TO 155
      K=2
      GO TO 163
C CHECK FOR INTERMEDIATE RIGHT INTERSECTION,EVALUATE IF REQUIRED
182 IF (ISR.NE.10) GO TO 162
      ISR=1
      GO TO 163
162 IF ((RAJR-RBJR)/(RAIR-RBIR).GT.0.0) GO TO 163
      AA=(AR2RJ-AR2K)/(RAJR-RAIR)
      BA=AR2R-AA*RAIR
      AB=(AR2RJ-AR2R)/(RBJR-RBIR)
      BB=AR2R-AB*RBIR
      RES1(K)=(BA-BA)/(AA-AB)
      RES2(K)=AA*RES1(K)+BA
      IF (K.EQ.2) GO TO 155
      K=2
C RE-INITIATE
163 AR2RJ=AR2R
      RAJL=RAIL
      RAJR=RAIR
      RBJL=RBIL
      RBJR=RBIR
140 CONTINUE
210 WRITE(6,210)
      FORMAT(' LOOP 140 THROUGH, NO POINTS FOUND')
      GO TO 155
195 IF (RES1(1).EQ.9000.0) GO TO 191
      IF (RES1(2).EQ.9000.0) GO TO 191
      IF (RES2(1).EQ.9000.0) GO TO 191
      IF (RES2(2).EQ.9000.0) GO TO 191
      GO TO 155
C EVALUATION OF INTERSECTIONS WHEN CURVES ARE ALMOST TANGENT
191 YGC=0.0
      CALL PENPTS(N2,N1,X3,Y3,Z3,HT1,YGC,APRES)
      R1=ABS(ARPLS(2)-APRES(1))/2
      CALL PENPTS(N2,N1,X4,Y4,Z4,HT2,YGC,APRES)
      R2=ABS(ARPLS(2)-APRES(1))/2
      RES2(1)=(R1**2)-(R2**2)+(ARP2**2)/(2.0*ARP2)
      RES2(2)=RES2(1)
      RES1(1)=SIGN(ABS((R1**2)-(RES2(1)**2)))
      RES1(2)=-RES1(1)
155 RETURN
      END
      SUBROUTINE PENPTS(NX,NY,X,Y,Z,HT,YG,XR)
      DIMENSION Y(40),ZX(40),Z(40,40),X(40),XR(10)
      IR=1
C SEARCH FOR J OF LOWER Y LINE
      DO 101 I=1,NY
      IF (Y(I).GE.YG) GO TO 102

```

INTO2810
 INTO2820
 INTO2830
 INTO2840
 INTO2850
 INTO2860
 INTO2870
 INTO2880
 INTO2890
 INTO2900
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 INTO2970
 INTO2980
 INTO2990
 INTO3000
 INTO3010
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 INTO3380
 INTO3390
 INTO3400
 INTO3410
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 INTO3430
 INTO3440
 INTO3450
 INTO3460
 INTO3470
 INTO3480
 INTO3490
 INTO3500

```

101 CONTINUE
102 J=I-1
C COARSE SCAN FOR ZERO PASS
C NEXT 4 LINES ARE EXECUTED IN FIRST SEARCH ONLY
YC=(Y(I)-Y(J))/(Y(J+1)-Y(J))
ZX(1)=(Z(I,J+1)-Z(I,J))*YC+Z(I,J)
IF(ZX(1).EQ.HT) GO TO 107
IB=2
112 DO 103 I=1,NX
    ZX(1)=(Z(I,J+1)-Z(I,J))*YC+Z(I,J)
    ZM=(Z(I,J+1)-Z(I-1,J))*(Y(I)-Y(J))/(Y(J+1)-Y(J))+Z(I-1,J)
    IF(ZX(1).EQ.HT) GO TO 108
    IF((ZX(I-1)-HT)/(ZX(1)-HT).LT.0.0) GO TO 104
103 CONTINUE
    GO TO 116
C CALCULATION OF PENETRATIONS IN EITHER TRIANGLE
104 XM=X(I-1)+(X(I)-X(I-1))*(Y(I)-Y(J))/(Y(J+1)-Y(J))
    IF(ZM.EQ.HT) GO TO 105
    IF((ZX(1)-HT)/(ZX(I)-HT).LT.0.0) GO TO 105
    DD=ABS(HT-ZM)+ABS(ZX(I-1)-HT)
    XS=X(I-1)+(X(I)-X(I-1))*ABS(ZX(I-1)-HT)/DD
    GO TO 110
105 XS=X(I)+(X(I)-XM)*ABS(ZM-HT)/(ABS(ZM-HT)+ABS(ZX(I)-HT))
    GO TO 110
C LOGICAL PENETRATIONS ACCUMULATION
107 XR(1)=X(I)
    I=1
    GO TO 113
108 XR(IR)=X(I)
    GO TO 111
110 XR(IR)=XS
111 IF(IR.EQ.2) GO TO 114
113 IR=2
    IR=I+1
    GO TO 112
116 IF(IR.EQ.1) GO TO 117
    XR(2)=1000.0
    GO TO 114
117 XR(1)=1000.0
    XR(2)=1000.0
114 RETURN
END
SUBROUTINE HITPLT(X,Y,Z,XS,YG,NX,IY,ZPRES)
C LINEAR INTERPOLATION ON CALIPRATION SURFACE TO EVALUATE
C CP VALUE AT CO-ORDINATES XS,YG. THE RESULT RETURNED IS ZPRES
C SEARCH FOR I OF LEFT X LINE
DO 1 IC=1,NX
    IF(X(IC).GE.XS) GO TO 2
1 CONTINUE
2 I=IC-1
C SEARCH FOR J OF LOWER Y LINE
DO 3 JC=1,IY
    IF(Y(JC).GE.YG) GO TO 4
3 CONTINUE
4 J=JC-1
    AL=(Y(J+1)-Y(J))/(X(I+1)-X(I))
    BL=Y(J)-AL*X(I)
    YCR=(AL*XS)+BL
    IF(YG.EQ.YCR) GO TO 7
    IF(YG.GT.YCR) GO TO 5
C RESULTING Z IS IN LOWER TRIANGLE
    X3=X(I+1)
    Y3=Y(J)
    Z3=Z(I+1,J)
    GO TO 6
C RESULTING Z IS IN UPPER TRIANGLE
5 X3=X(I)
    Y3=Y(J+1)
    Z3=Z(I,J+1)

```

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INT03510
INT03520
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INT03600
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INT03990
INT04000
INT04010
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INT04070
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INT04090
INT04100
INT04110
INT04120
INT04130
INT04140
INT04150
INT04160
INT04170
INT04180
INT04190
INT04200

```

C GENERAL CALCULATION: GOOD FOR BOTH TRIANGLES

```

6  GENRAL CALCULATION USED FOR BOTH PROBLEMS
      X1=X(I)
      Y1=Y(J)
      Z1=Z(I,J)
      X2=X(I+1)
      Y2=Y(J+1)
      Z2=Z(I+1,J+1)
      AP=((Z1-Z3)*(Y1-Y2)-(Z1-Z2)*(Y1-Y3))/((X1-X3)*(Y1-Y2)-(X1-X2)
1* (Y1-Y3))
      BP=((Z1-Z2)-AP*(X1-X2))/(Y1-Y2)
      CP=Z1-AP*(1-BP*Y1)
      ZRES=AP*(G+BP*Y2+CP)
      GO TO 100

```

```

7      ZRFS=(Z(I+1,J+1)-Z(I,J))*((X(J)-X(I))/(X(I+1)-X(I))+Z(I,J))
100    RETURN

```

C EVALUATION OF MAXIMUM OF OF CALIBRATION SURFACE MATRIX
DIMENSION Z(40,40)

SUBROUTINE MINARY(Z,ZMIN,VX,VY)

C EVALUATION OF MINIMUM OF OF CALIBRATION SURFACE MATRIX
 DIMENSION Z(40,40)

```

DO 1 I=1,NX
DO 1 J=1,NY
1 IF(Z(I,J).LE.ZMIN) ZMIN=Z(I,J)
RETURN
END

```

C END OF WVDR

INTC4210
INTC4220
INTC4230
INTC4240
INTC4250
INTC4260
INTC4270
INTC4280
INTC4290
INTC4300
INTC4310
INTC4320
INTC4330
INTC4340
INTC4350
INTC4360
INTC4370
INTC4380
INTC4390
INTC4400
INTC4410
INTC4420
INTC4430
INTC4440
INTC4450
INTC4460
INTC4470
INTC4480
INTC4490
INTC4500
INTC4510
INTC4520
INTC4530
INTC4540
INTC4550

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